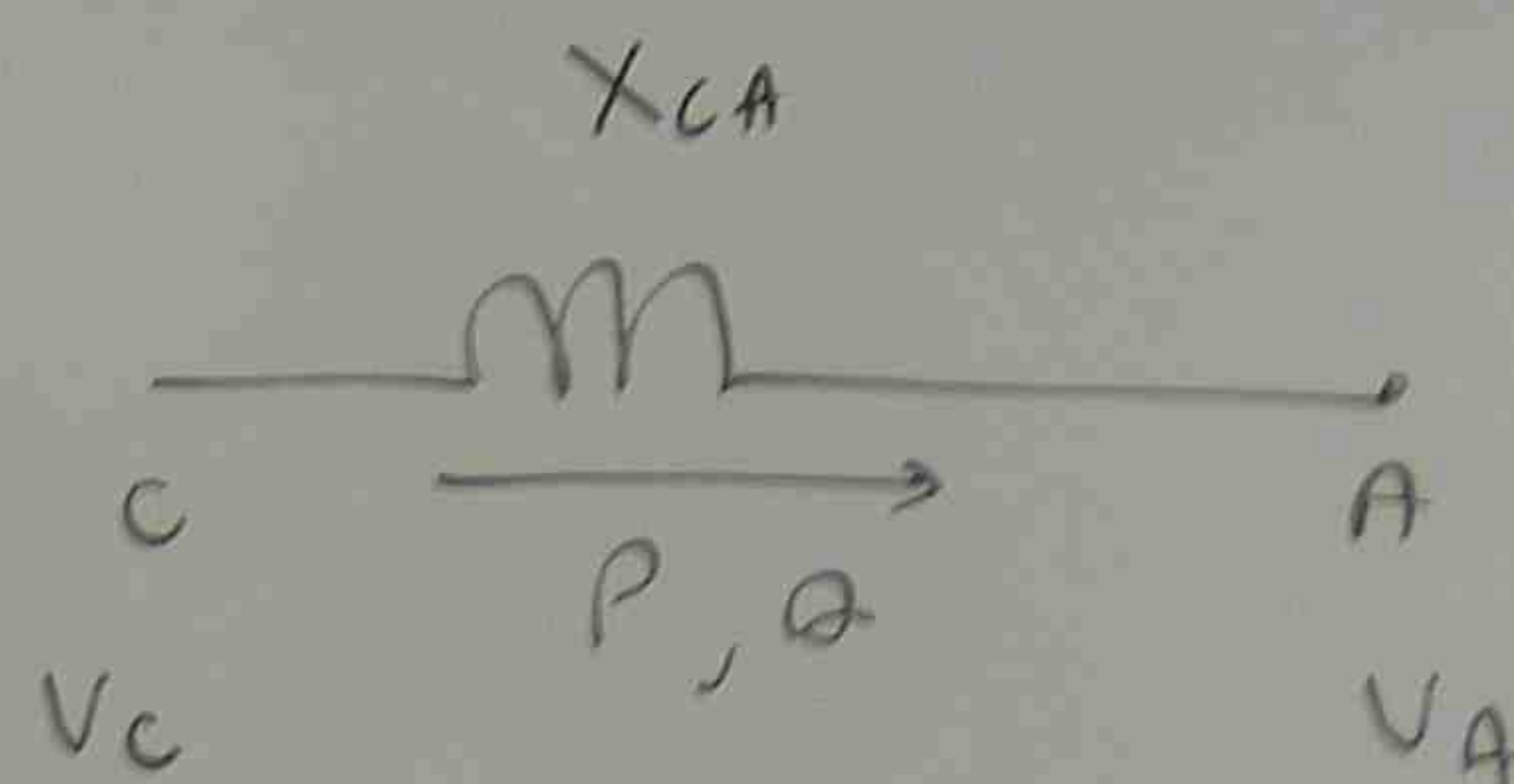


VOLTAGE & POWER FLOW RELATIONSHIP



V_A = VOLTAGE AT POINT (A) (RECEIVING END VOLTAGE)

V_C = VOLTAGE AT POINT (C) (SENDING END VOLTAGE)

X_{CA} = INDUCTIVE REACTANCE BETWEEN A & C

P = ACTIVE POWER FLOW FROM C TO A (WATT)

Q = REACTIVE POWER FLOW FROM C TO A (VAR)

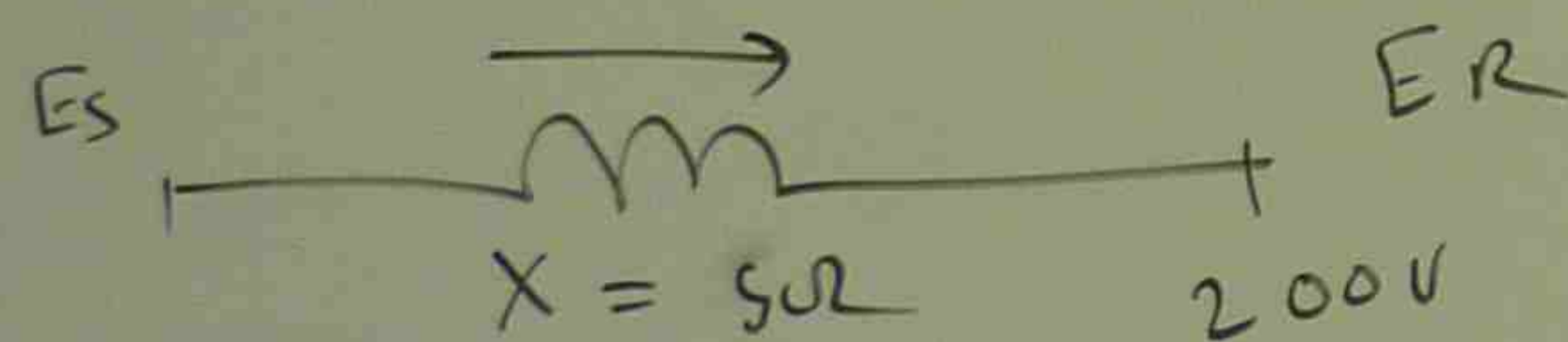
P_h

E_s

$E_s = \sqrt{\dots}$

$$V_C = \sqrt{\left(V_A + \frac{Q X_{CA}}{V_A}\right)^2 + \left(\frac{P X_{CA}}{V_A}\right)^2}$$

Ph



$$P = 1000 \text{ WATT}$$

$$Q = 500 \text{ VAR}$$

Find E_S

$$E_S = \sqrt{\left(E_R + \frac{Q X}{E_R}\right)^2 + \left(\frac{P X}{E_R}\right)^2}$$

$$E_S = \sqrt{\left(200 + \frac{500 \times 5}{200}\right)^2 + \left(\frac{1000 \times 5}{200}\right)^2}$$

$$= \sqrt{(200 + 12.5)^2 + (25)^2}$$

$$= \sqrt{212.5^2 + 25^2}$$

$$= 213.9V$$

END VOLTAGE)
END VOLTAGE)
P C
A (WATT)
A (VAR)

P=AC
Q=V
Q (VAR)
Power
Active Power
IN
React

$$\left(\frac{X_{CA}}{VA} \right)^2$$

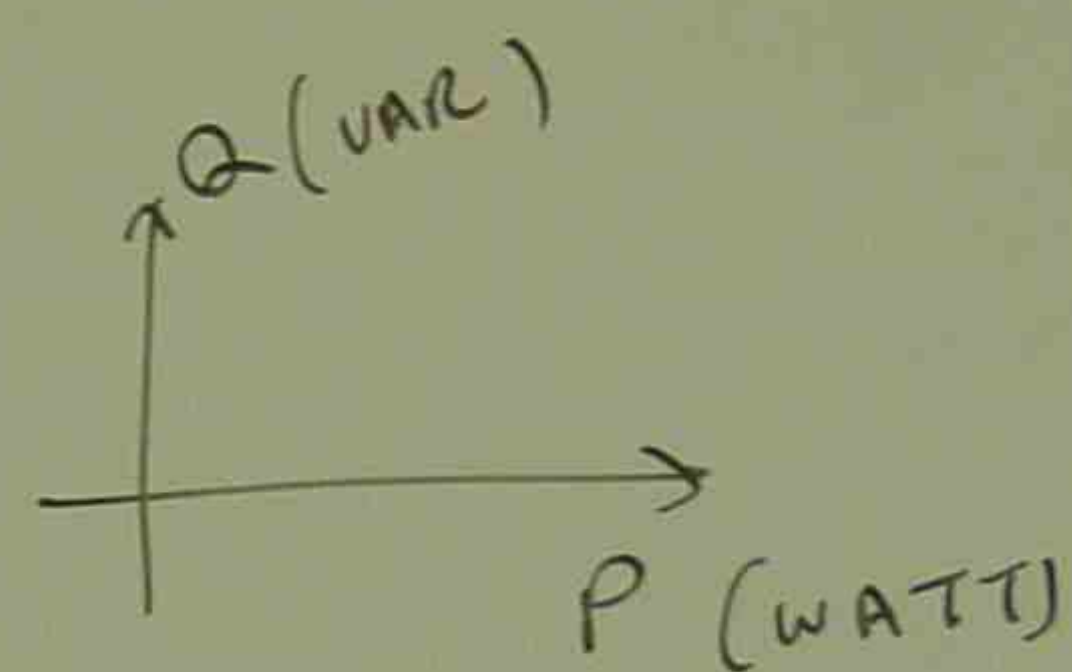
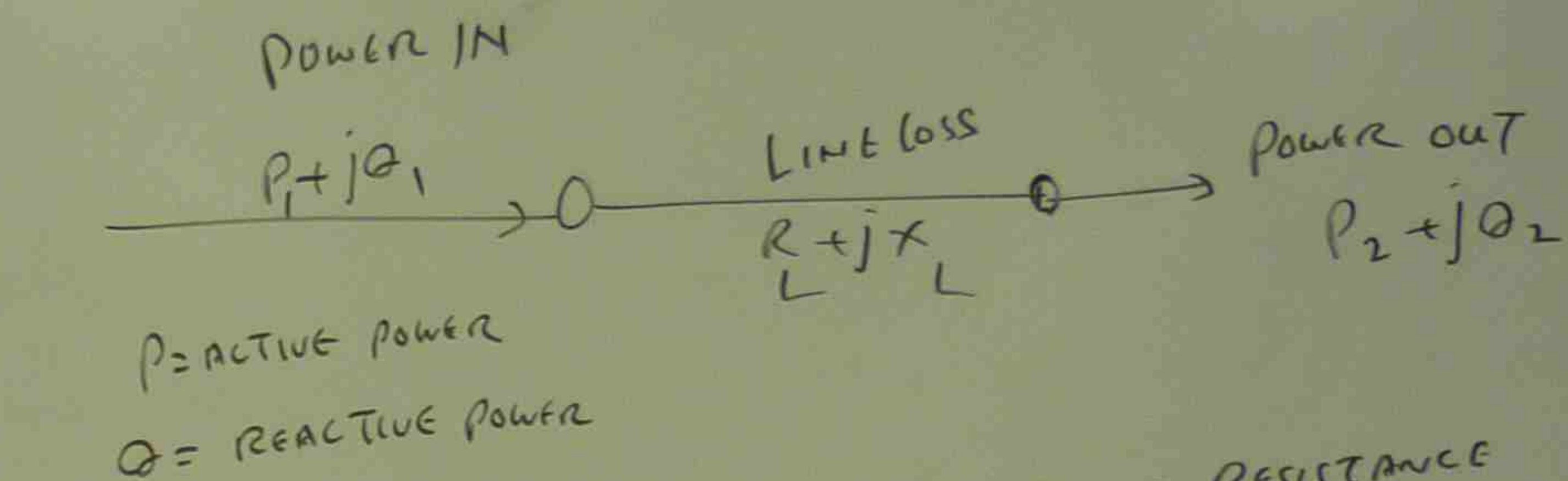
$$E_S = \sqrt{\left(200 + \frac{500 \times 5}{200}\right)^2 + \left(\frac{1000 \times 5}{200}\right)^2}$$

$$= \sqrt{(200 + 12.5)^2 + (25)^2}$$

$$= \sqrt{212.5^2 + 25^2}$$

$$= 213.9 \text{ V}$$

$$\left(\frac{P \times X}{E_R} \right)^2$$



$R_L = \text{LINE RESISTANCE}$
 $X_L = \text{LINE INDUCTIVE REACTANCE}$
 $I = \text{LINE CURRENT}$

$$\text{POWER IN} = \text{POWER OUT} + \text{LINE LOSS}$$

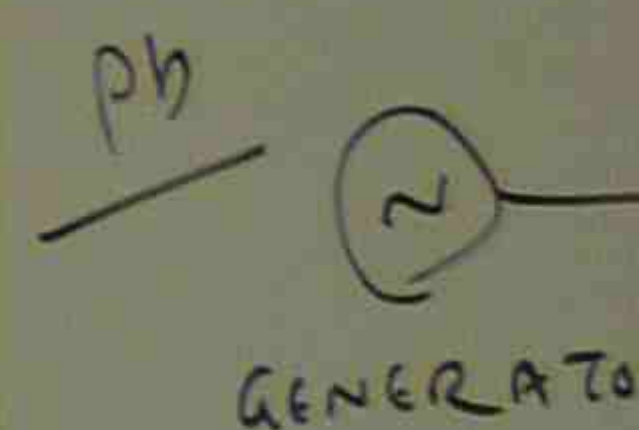
$$\text{ACTIVE POWER INPUT} = \text{ACTIVE POWER OUTPUT} + \text{ACTIVE POWER LOSS}$$

$$P_1 = P_2 + I^2 R$$

$$\text{REACTIVE POWER INPUT} = \text{REACTIVE POWER OUTPUT} + \text{REACTIVE POWER LOSS}$$

$$Q_1 = Q_2 + I^2 X$$

LINE C

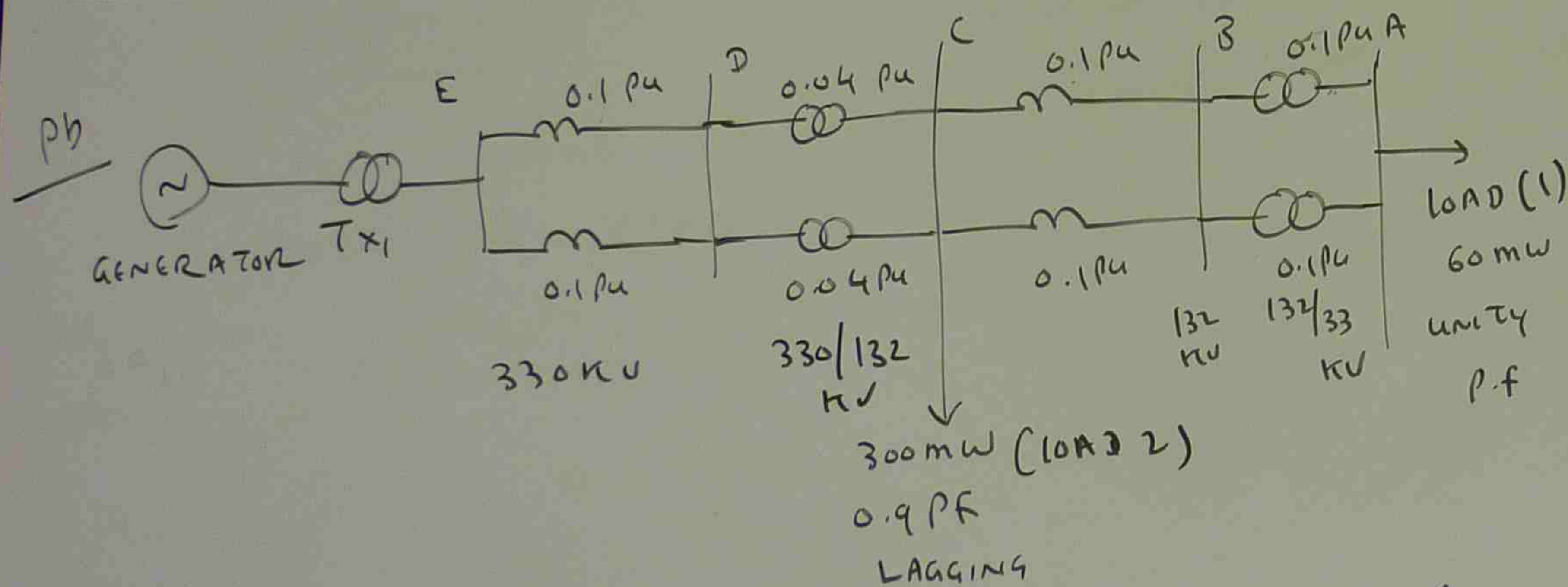


FIND

$Z(p$

$$I_{\text{LINE CURRENT}} = \frac{\text{ACTIVE POWER LOSS} + j \text{ REACTIVE POWER LOSS}}{\text{RECEIVING END VOLTAGE}}$$

$$Z = \frac{\sqrt{(\text{ACTIVE POWER LOSS})^2 + (\text{REACTIVE POWER LOSS})^2}}{\text{RECEIVING END VOLTAGE}}$$



FIND (a) GENERATOR VOLTAGE (b) ACTIVE & REACTIVE
POWER SUPPLIED BY GENERATOR

$$Z(\text{pu}) = \frac{Z(\Omega) \times \text{BASE VA}}{(\text{BASE VOLTAGE})^2}$$

BASE = 100 mW \rightarrow 1 pu

LOAD power = 0.6 pu unity PF

$$\cos \theta = 1$$

$$Q = 0$$

$$\sin \theta = 0$$

LOAD ACTIVE POWER = 0.6 pu

$$\text{LOAD REACTIVE POWER} = \text{LOAD ACTIVE POWER} \tan \phi$$

$\frac{1}{2} \quad 0.6 \text{ km}$

$$= 0$$

LOAD (2) AT (C) POINT

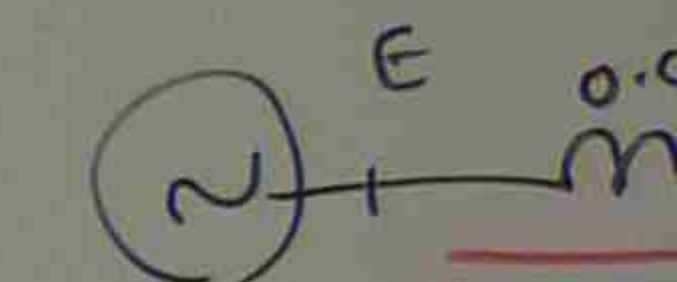
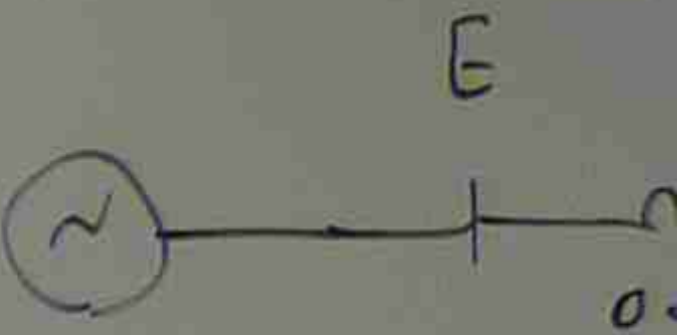
$P_f = 0.9$ LAGGING

$$\cos \theta = 0.9 \rightarrow \theta = \cos^{-1} 0.9 = 26$$

LOAD (2) ACTIVE POWER:- 3 Ph

REACTIVE POWER = 3 dm 26

$\therefore 1.46 \text{ p.u.}$



$E_S = ?$
 P_{EL}
 Q_{EL}

$$E_c = \int (v$$

$$V_A = 1 \text{ pu}$$

$$E_c = \int (1 -$$

$$\sqrt{1}$$

$\sqrt{1}$

$$\text{BASE} = 100 \text{ MW} \rightarrow 1 \text{ pu}$$

$$\text{LOAD POWER} = 0.6 \text{ pu} \quad \text{UNITY PF}$$

$$\cos \theta = 1$$

$$\theta = 0$$

$$\sin \theta = 0$$

$$\text{LOAD ACTIVE POWER} = 0.6 \text{ pu}$$

$$\text{LOAD REACTIVE POWER} = \text{LOAD ACTIVE POWER} \tan \theta$$

$$= 0.6 \tan 0$$

$$= 0$$

LOAD (2) AT (C) POINT

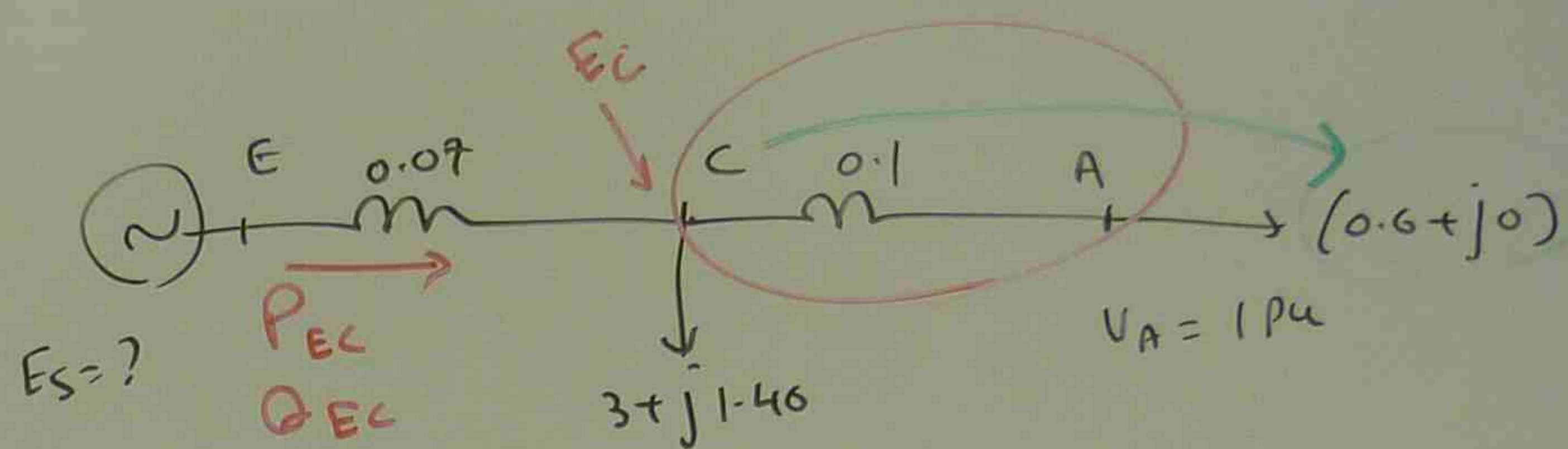
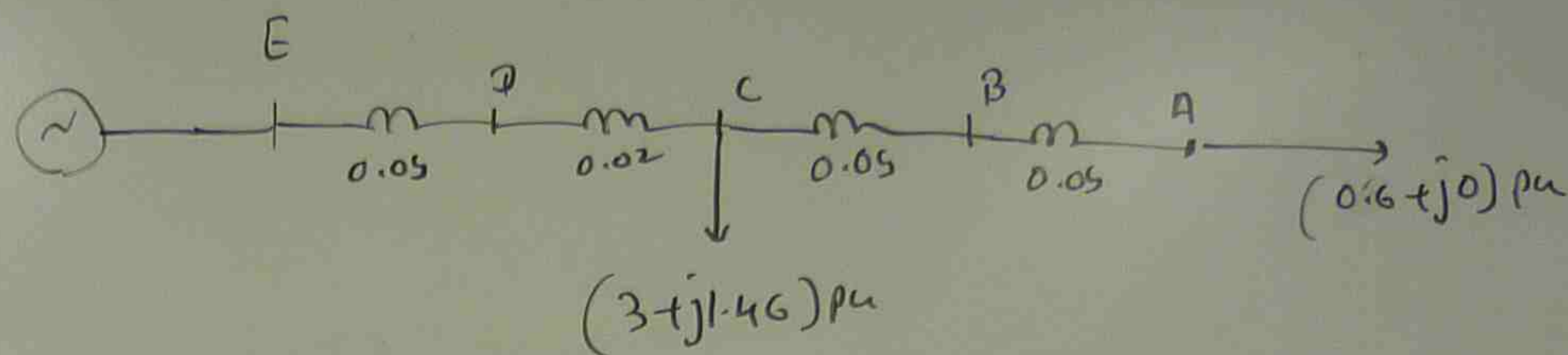
$$\text{PF} = 0.9 \text{ LAGGING}$$

$$\cos \theta = 0.9 \rightarrow \theta = \cos^{-1} 0.9 = 26$$

$$\text{LOAD (2) ACTIVE POWER} = 3 \text{ pu}$$

$$\text{REACTIVE POWER} = 3 \tan 26$$

$$= 1.46 \text{ pu}$$



$$E_C = \sqrt{\left(V_A + \frac{Q_{CA} X_{CA}}{V_A}\right)^2 + \left(\frac{P_{CA} X_{CA}}{V_A}\right)^2}$$

$$V_A = 1 \text{ pu} \quad X_{CA} = 0.1 \text{ pu} \quad P_{CA} = 0.6, \quad Q_{CA} = 0$$

$$E_C = \sqrt{\left(1 + \frac{0 \times 0.1}{1}\right)^2 + \left(\frac{0.6 \times 0.1}{1}\right)^2}$$

$$= \sqrt{1^2 + (0.06)^2}$$

$$= \sqrt{1 + 3.6 \times 10^{-3}} = \sqrt{1.0036} = 1.001$$

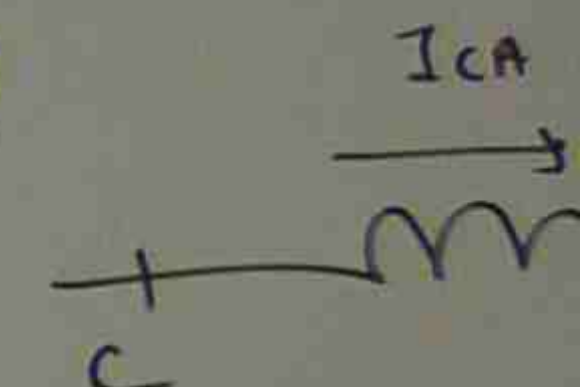
$$E_S = \sqrt{\left(E_C + \frac{Q_{EC} X_{EC}}{E_C}\right)^2 + \left(\frac{P_{EC} X_{EC}}{E_C}\right)^2}$$

$$E_C = 1.001 \text{ pu} \quad X_{EC} = 0.07 \text{ pu}$$

$$P_{EC} = P_{CA} + I_{CA}^2 R_{EC}$$

$$Q_{EC} = Q_{CA} + I_{CA}^2 X_{EC}$$

$$I_{CA} = ?$$

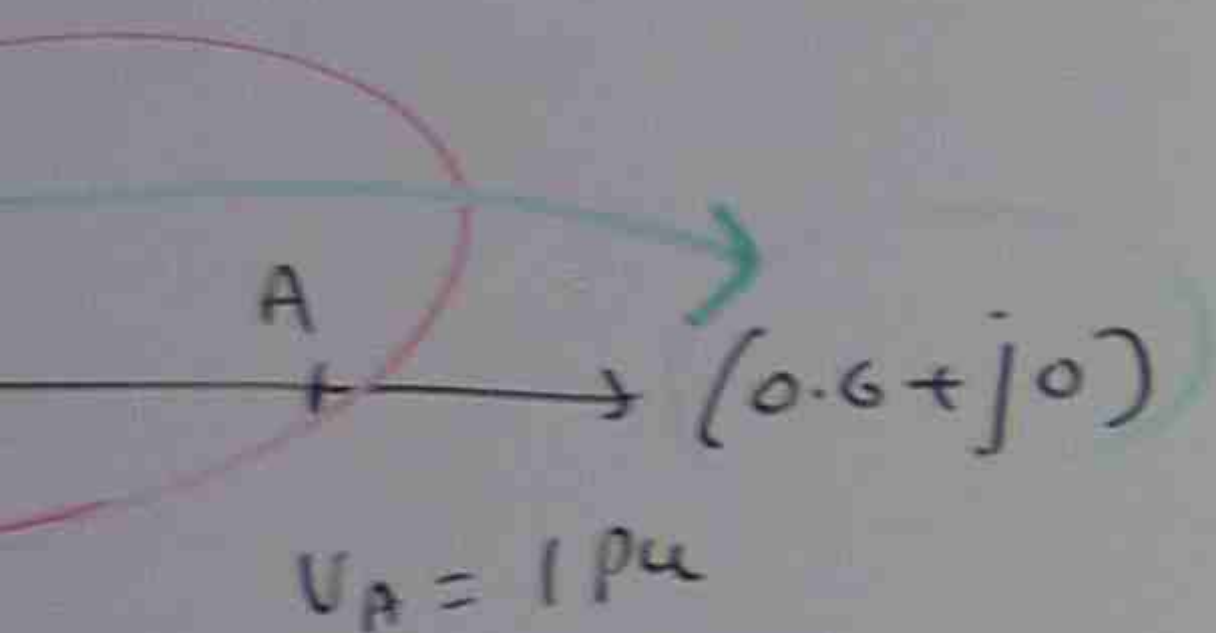
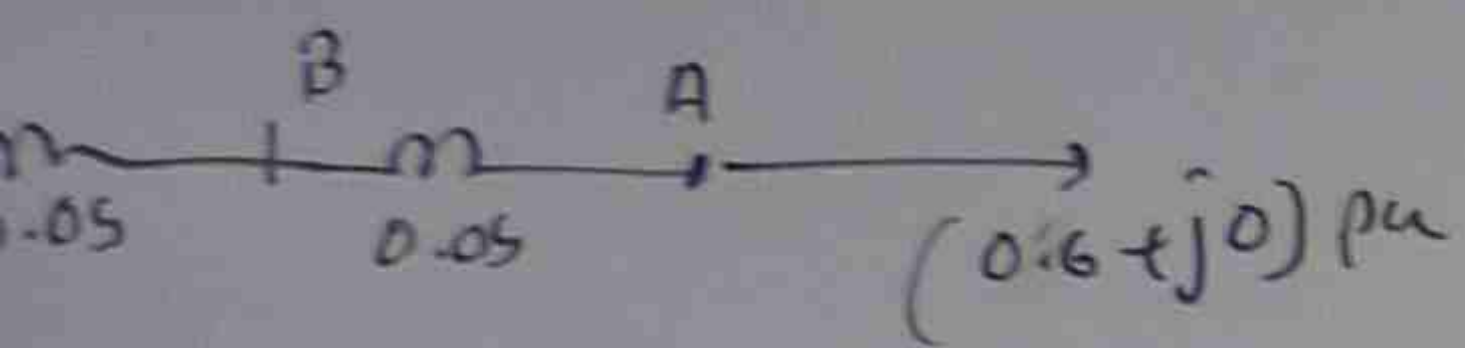


$$I_{CA} = \sqrt{\frac{0.6^2 + 0^2}{1}}$$

$$P_{EC} = P_{CA} + I_{CA}^2 R_{EC}$$

$$Q_{EC} = Q_{CA} + I_{CA}^2 X_{EC}$$

$$E_S = \sqrt{\left(1.001 + \frac{1.4}{1.001}\right)^2 + \left(\frac{0.6}{1.001}\right)^2}$$



$$+ \left(\frac{P_{C \rightarrow A} X_{CA}}{V_A} \right)^2$$

$$P_{CA} = 0.6, Q_{CA} = 0$$

$$\left(\frac{0.6 \times 0.1}{1} \right)^2$$

$$= 1.001$$

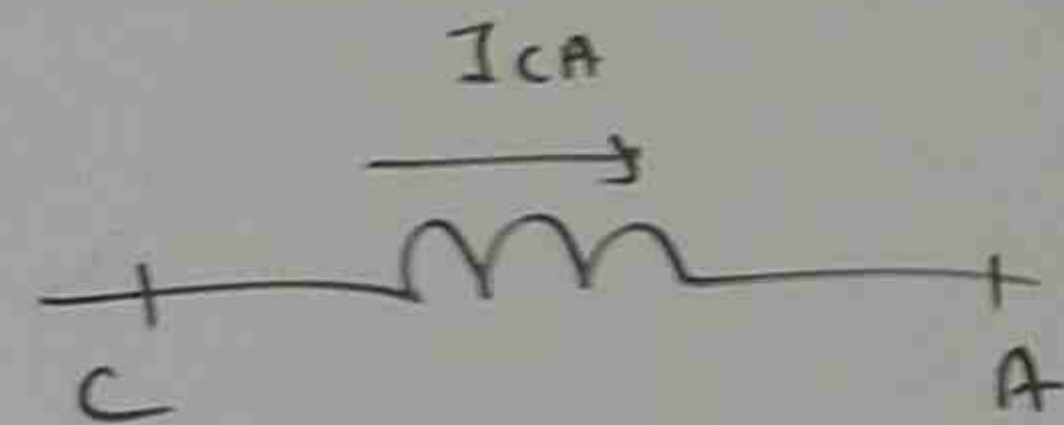
$$E_s = \sqrt{\left(E_c + \frac{Q_{Ec} X_{Ec}}{E_c} \right)^2 + \left(\frac{P_{Ec} X_{Ec}}{E_c} \right)^2}$$

$$E_c = 1.001 \text{ pu}, X_{Ec} = 0.07, P_{Ec} = ?, Q_{Ec} = ?$$

$$P_{Ec} = P_{CA} + I_{CA}^2 R_{CA} + P_C$$

$$Q_{Ec} = Q_{CA} + I_{CA}^2 X_{CA} + Q_C$$

$$I_{CA} = ?$$



$$I_{CA} = \frac{\sqrt{(\text{Active power loss } C-A)^2 + (\text{Reactive power loss } C-A)^2}}{V_A}$$

$$I_{CA} = \frac{\sqrt{0.6^2 + 0^2}}{1} = \frac{\sqrt{0.6^2}}{1} = 0.6 \text{ pu}$$

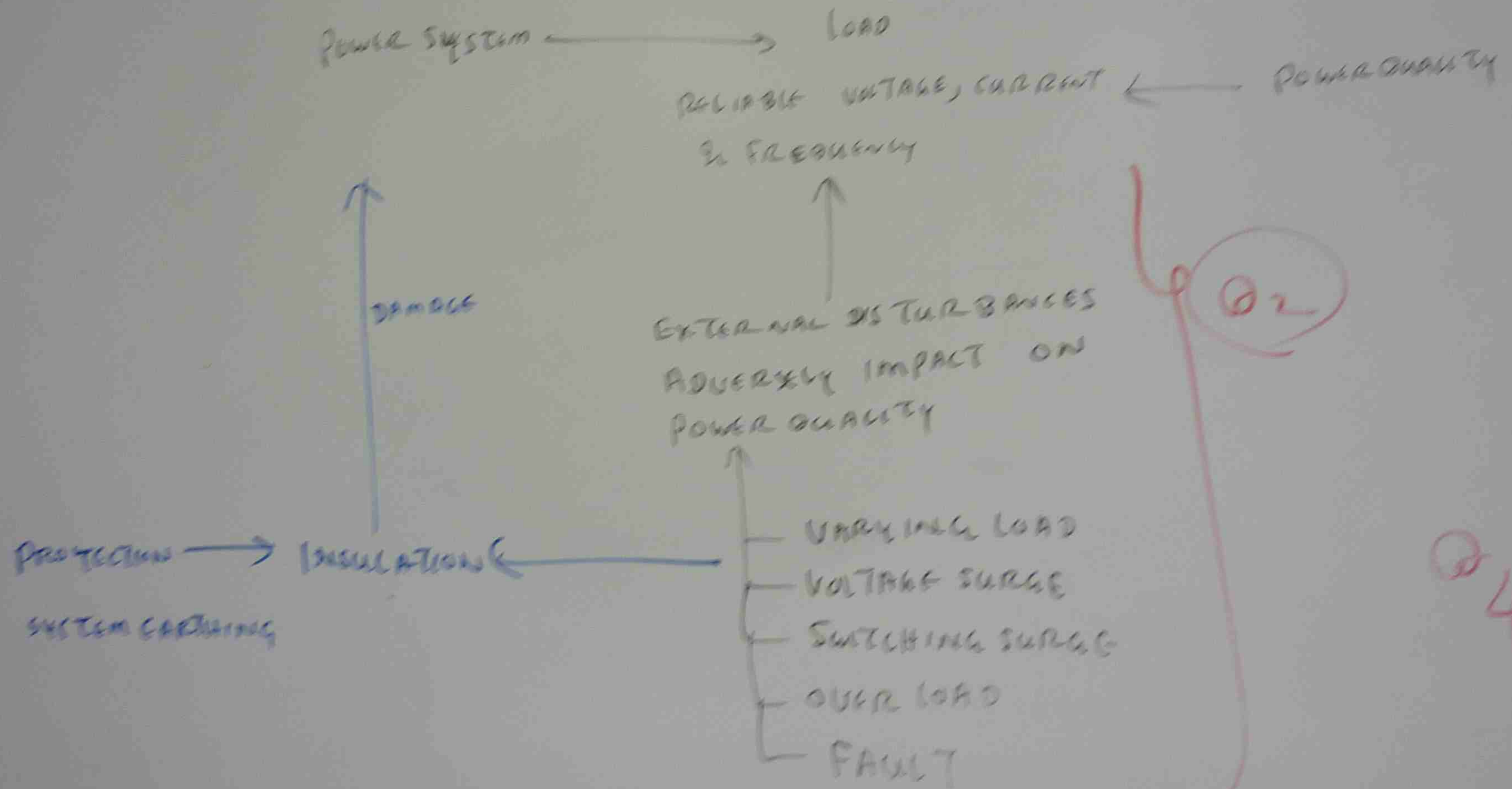
$$P_{Ec} = P_{CA} + I_{CA}^2 R_{CA} + P_C = 0.6 + (0.6)^2 \times 0 + 3 = 3.6$$

$$Q_{Ec} = Q_{CA} + I_{CA}^2 X_{CA} + Q_C = 0 + (0.6)^2 \times 0.1 + 1.46 = 0.036 + 1.46 = 1.496 \text{ pu}$$

$$E_s = \sqrt{\left(1.001 + \frac{1.496 \times 0.07}{1.001} \right)^2 + \left(\frac{3.6 \times 0.07}{1.001} \right)^2} = \sqrt{(1.001 + 0.1046)^2 + (0.251)^2}$$

$$= \sqrt{1.11^2 + 0.251^2} = \sqrt{1.3005} = 1.14 \text{ pu}$$

G037 + G038 + G039 SUPPLEMENTARY NOTES



INSULATION
 SEPARATION
 FACTOR
 - CHE
 - DE
 - LIC
 T
 H

Supplementary Notes

LOAD
VOLTAGE, CURRENT ← POWER QUALITY
Efficiency

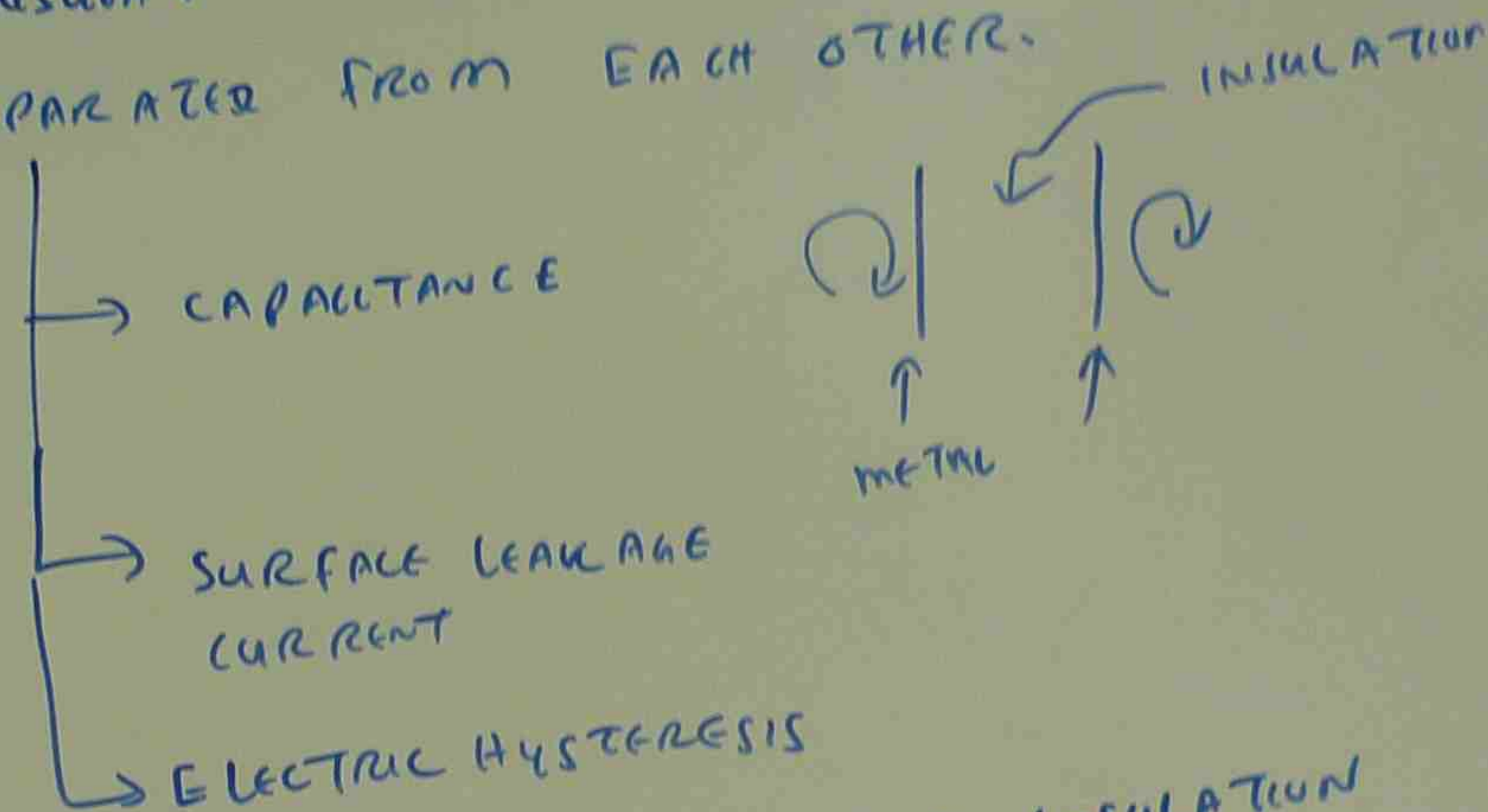
DISTURBANCES
IMPACT ON
QUALITY

CHANGING LOAD
VOLTAGE SURGE
SWITCHING SURGE
OVER LOAD
FAULT

Q2

INSULATION

INSULATION IS REQUIRED TO KEEP ELECTRICAL CONDUCTORS SEPARATED FROM EACH OTHER.



FACTORS THAT DETEORATE THE INSULATION

- CHEMICAL IMPACT
- DENSITY DECREASES → DOWN GRADE THE QUALITY OF GASEOUS INSULATION
- LIGHTNING
- TRAVELLING VOLTAGE SURGE
- HARMONIC

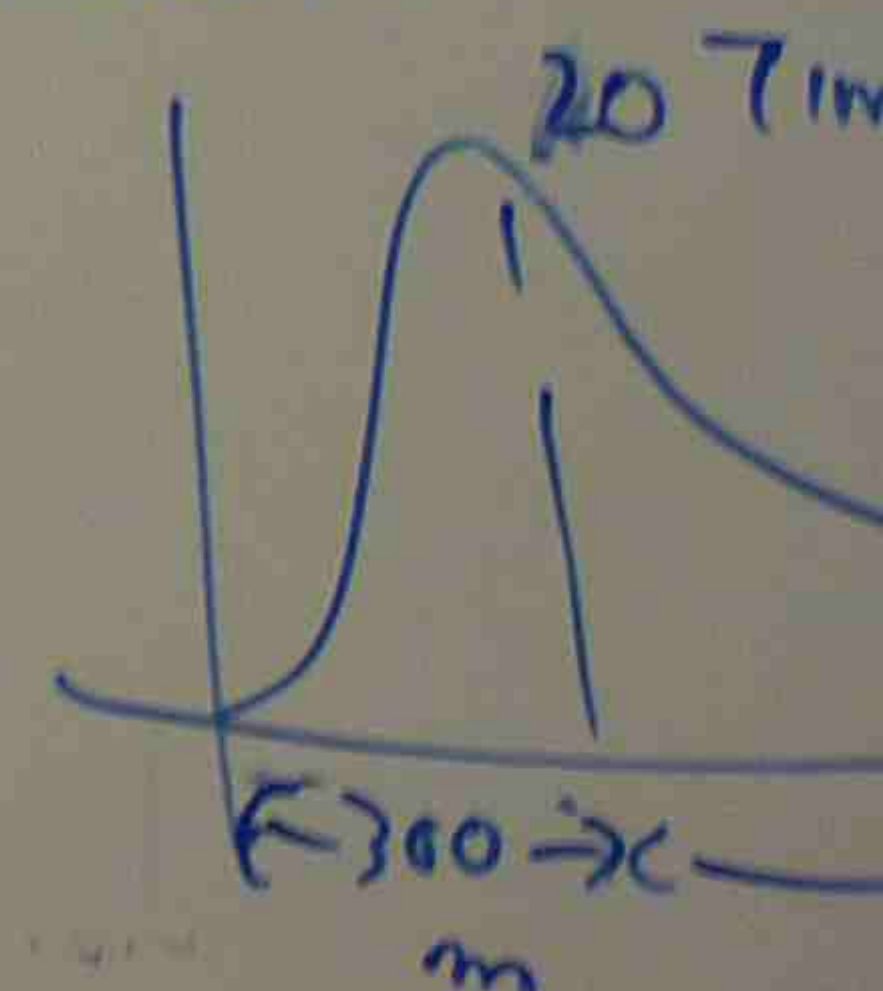
Q4

Sf6

TO PROTECT THE
FOLLOWING ACTIONS

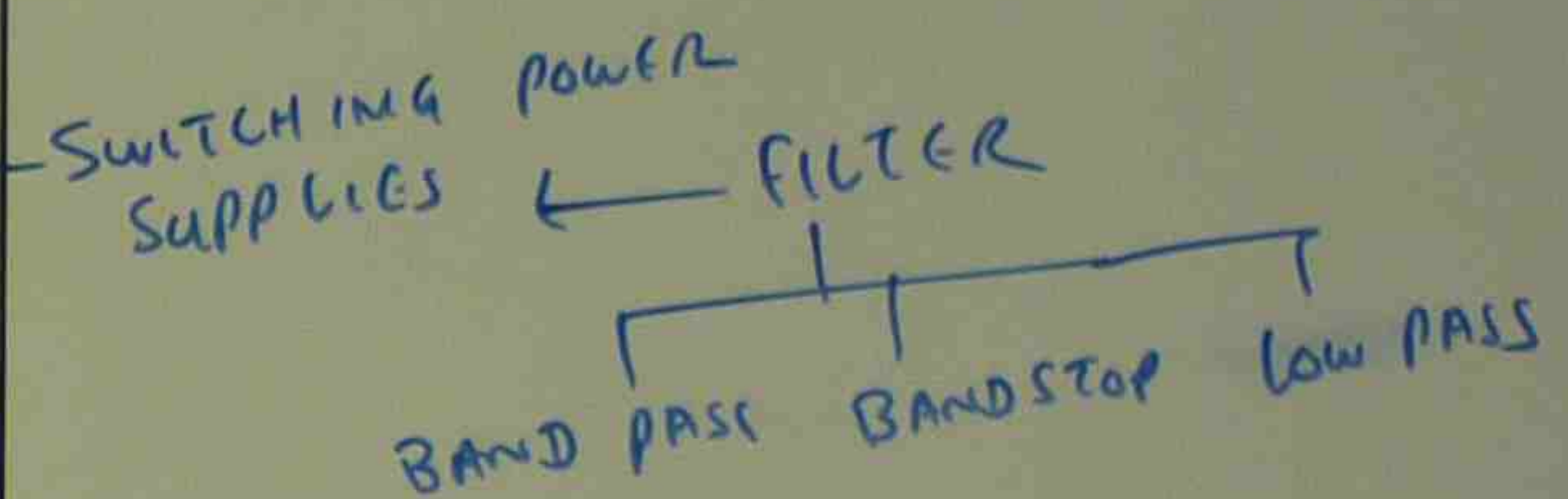
- (1) INVESTIGATION AND PROTECTION
- (2) PROTECT
- (3) STUDY THE EFFECT OF INSULATION REINFORCEMENT
- (4) PROVIDE AND L

LIGHTNING STRIKE INSULATION



Q3
 TO PROTECT THE INSULATION FROM EXTERNAL DAMAGING IMPACTS, THE FOLLOWING ACTIONS ARE REQUIRED

- (1) INVESTIGATE THE SOURCE OF ELECTRICAL INTERFERENCES AND PROVIDE APPROPRIATE SHIELDING (OR) PROTECTION
- (2) PROTECT FROM TRAVELLING WAVE FORM / HARMONIC PROTECTION
- (3) STUDY THE BREAK DOWN VOLT-TIME CHARACTERISTICS OF INSULATION & FIND OUT THE EARLY SIGNS OF INSULATION DEGRADATION. PROVIDE APPROPRIATE REINFORCEMENT
- (4) PROVIDE APPROPRIATE PROTECTION FOR CHEMICAL AND LEAKAGE.

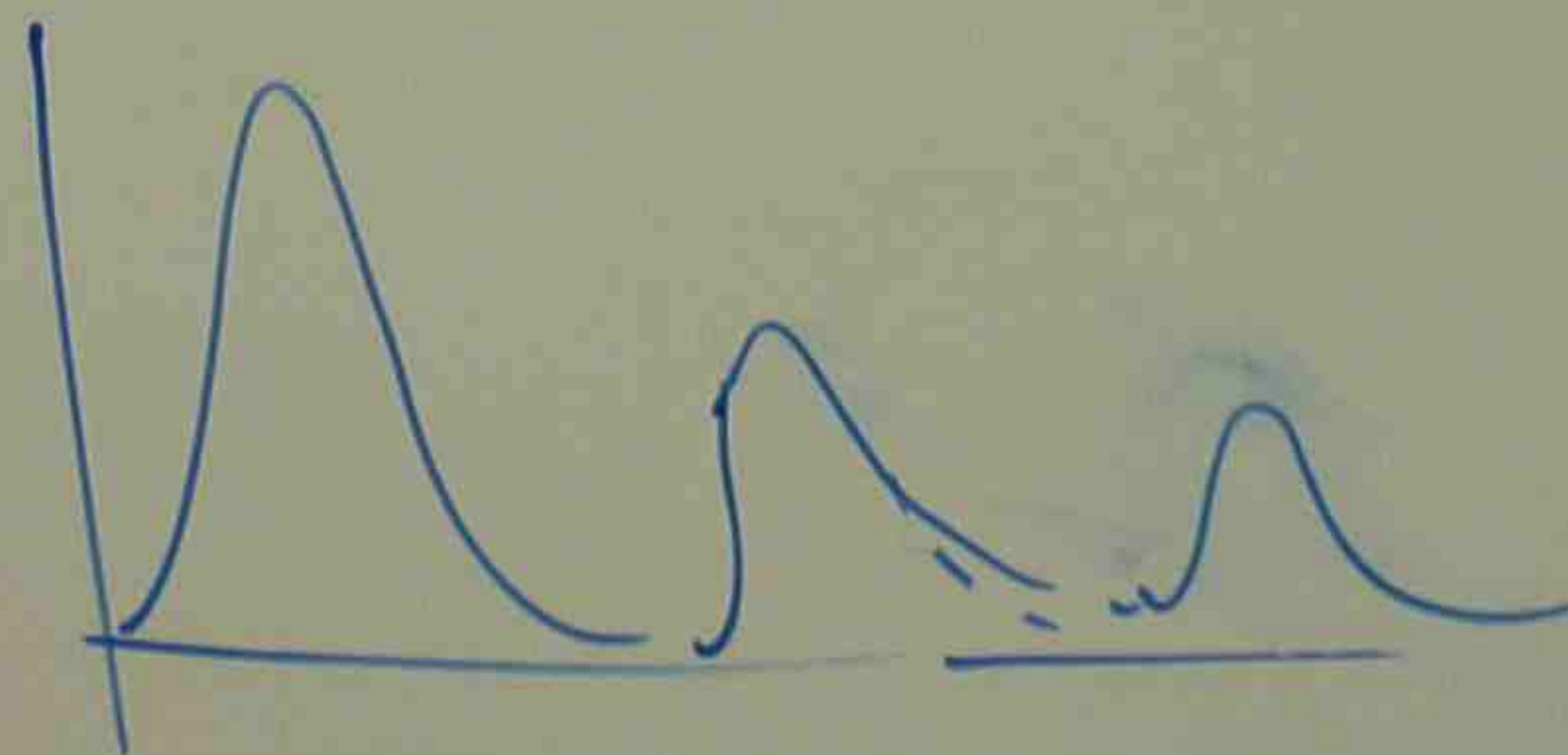
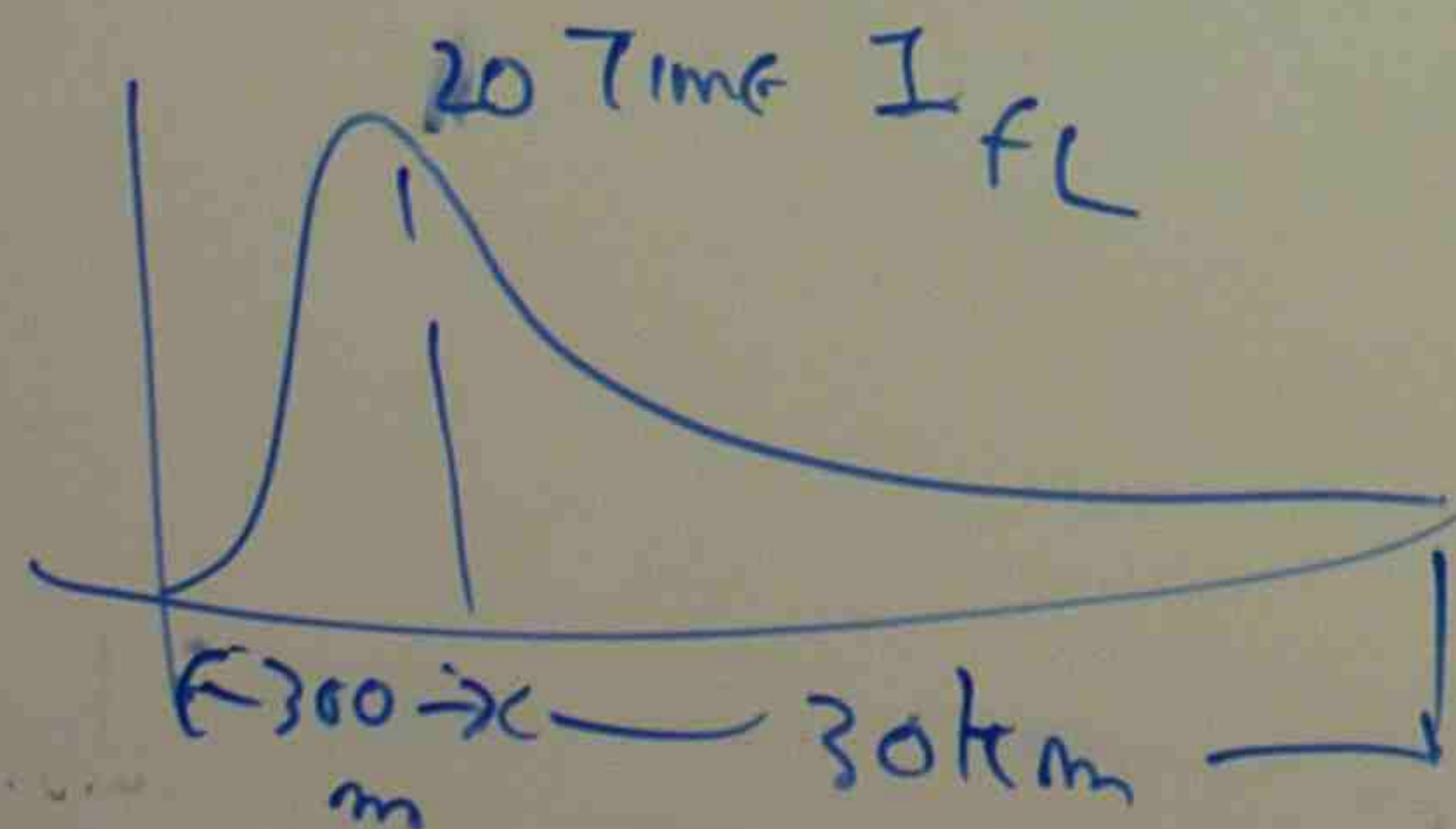


THE INSULATION MUST POSSESS THE CAPACITY TO WITHSTAND THE ABNORMAL PEAK VOLTAGE FOR FIRST A FEW SECONDS.

AS 1768-1991

INSULATION MUST COMPLY WITH AS 1768 WAVE-FORM STANDARD

Sf6
 LIGHTNING STRIKES CAN SEVERELY DAMAGE THE INSULATION



SWITCHING M...

THE SWITCHIN
 APPROPRIATE
 SURGES

Q1 WHAT

POWER C
 FREQU

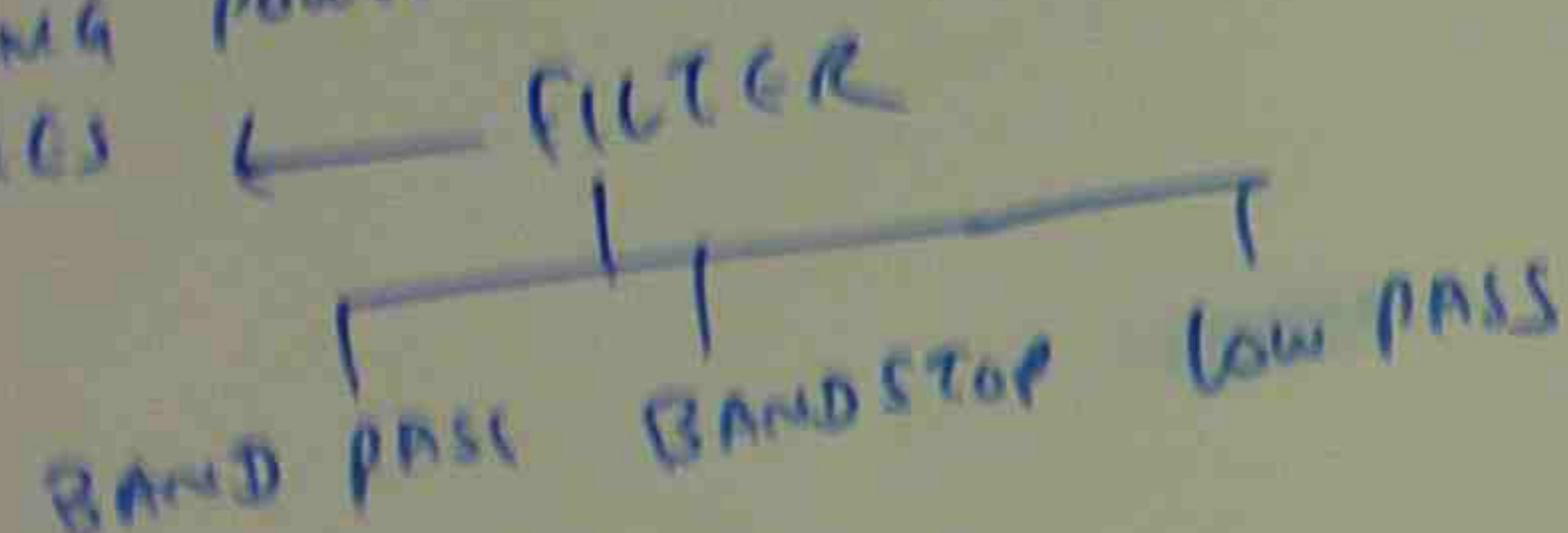
Q2 WHAT

Q3 W

Q4 W

Q5

SWITCHING power
SUPPLIES



THE INSULATION MUST POSSES THE CAPACITY TO WITHSTAND THE ABNORMAL PEAK VOLTAGE FOR FIRST A FEW SECOND.

AS 1768-1991

INSULATION MUST COMPLY WITH

AS 1768 WAVE FORM STANDARD

SWITCHING MODE POWER SUPPLIES

THE SWITCHING power SUPPLIES CAN PRODUCE THE SWITCHING SURGES. APPROPRIATE FILTER MUST BE UTILIZED TO REMOVE THE SWITCHING SURGES

Q1 WHAT IS POWER QUALITY?

POWER QUALITY IS RELIABLE VOLTAGE, CURRENT AND FREQUENCY OF POWER SYSTEM

Q2 WHAT FACTORS CAN DAMAGE THE POWER QUALITY?

Q3 WHAT IS INSULATION?

Q4 WHAT ARE THE FACTORS THAT CAN DAMAGE INSULATION?

Q5 WHAT ACTIONS ARE REQUIRED TO PROTECT THE INSULATION FROM EXTERNAL DAMAGING IMPACTS

SITE EARTHING & SURGE PROTECTION

THE MAIN OBJECTIVES OF SITE EARTHING

- ① TO AVOID PHYSICAL DAMAGE TO BUILDING AND EQUIPMENTS DUE TO DIRECT AND INDIRECT LIGHTNING STRIKES AND SYSTEM FAULT SURGES
- ② TO PROVIDE SAFE WORKING ENVIRONMENT FOR PERSONNEL DURING LIGHTNING STRIKE
- ③ TO PROVIDE SHIELDING AND ALTERNATIVE PATH FOR INDUCED CURRENT TO REDUCE THE EFFECT OF COUPLED NOISE ON ELECTRONIC EQUIPMENTS
- ④ TO PROVIDE AN EQUIPOTENTIAL PLATFORM ON WHICH ELECTRONIC EQUIPMENTS CAN OPERATE WITHOUT LARGE DIFFERENTIAL VOLTAGE

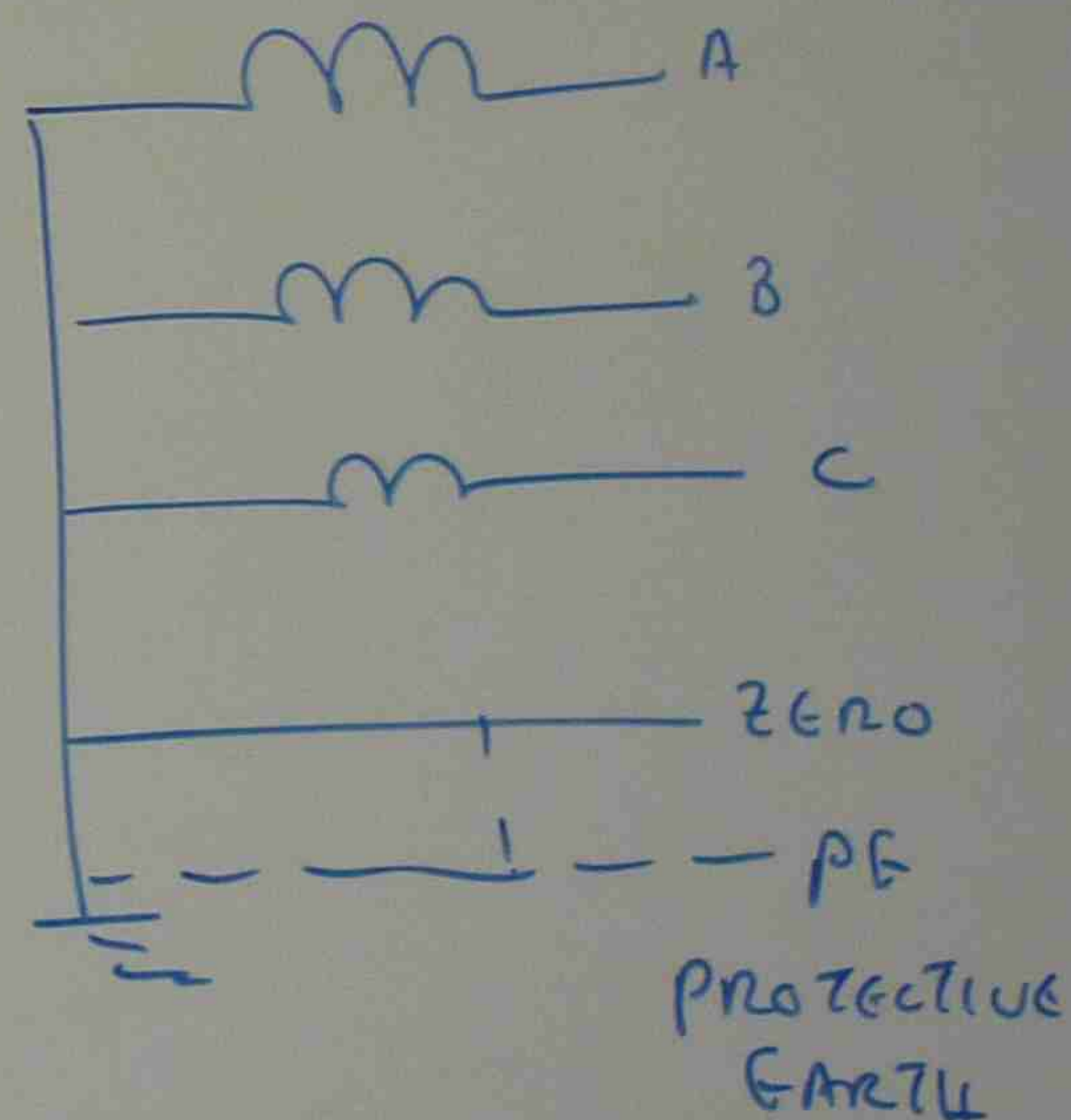
TOUCH VOLTAGE — VOLTAGE BETWEEN EQUIPMENT & EARTH

STEP VOLTAGE — POTENTIAL DIFFERENCE IN 1m FOOTSTEP

MESH VOLTAGE — MAXIMUM TOUCH VOLTAGE IN EARTHING GRID

PROTECTIVE EARTH
ALL EXPOSED TERMINALS AT SAME VOLTAGE LEVEL

FUNCTIONAL EARTH
PROTECTION AGAINST ELECTRIC SHOCK



Q6 WHAT OF SITE

Q7 EXPLA STEP U

Q8 WHAT AND

PROTECTION

OF SITE EARTHING

DAMAGE TO BUILDING AND EQUIPMENTS
INDIRECT LIGHTNING STRIKES AND
WORKING ENVIRONMENT FOR PERSONNELS
STRIKE

ELDING AND ALTERNATIVE PATH FOR
TO REDUCE THE EFFECT OF
ON ELECTRONIC EQUIPMENTS
AN EQUIPOTENTIAL PLATFORM ON
NIC EQUIPMENTS CAN OPERATE
DGE DIFFERENTIAL VOLTAGE

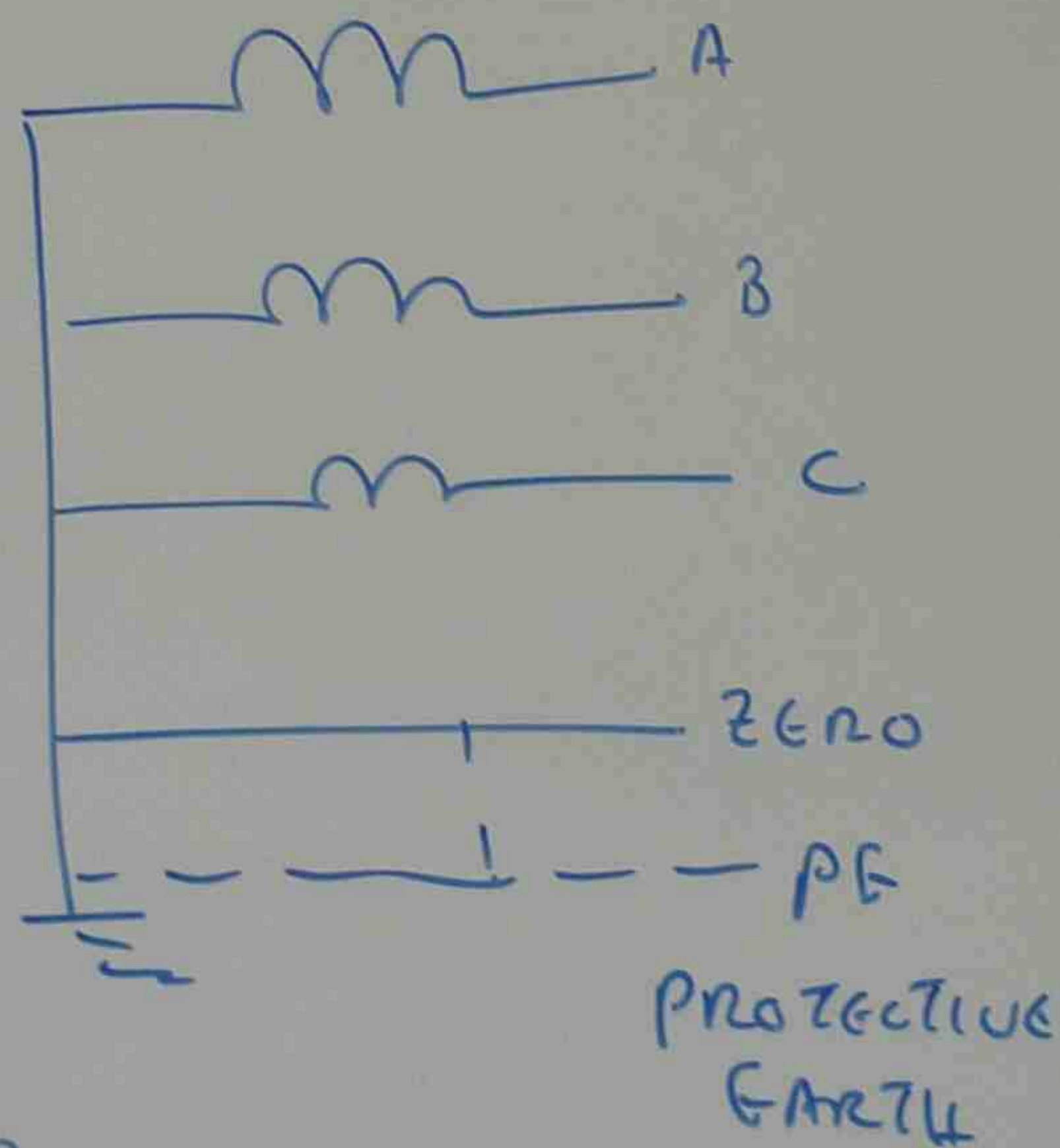
VOLTAGE — VOLTAGE BETWEEN EQUIPMENT &
EARTH

AGE — POTENTIAL DIFFERENCE IN 1m FOOT STEP

STAGE — MAXIMUM TOUCH VOLTAGE IN
EARTHING GRID

PROTECTIVE EARTH
ALL EXPOSED TERMINALS AT
SAME VOLTAGE LEVEL

FUNCTIONAL EARTH
PROTECTION AGAINST ELECTRIC
SHOCK



Q6 WHAT ARE THE MAIN OBJECTIVES
OF SITE EARTHING

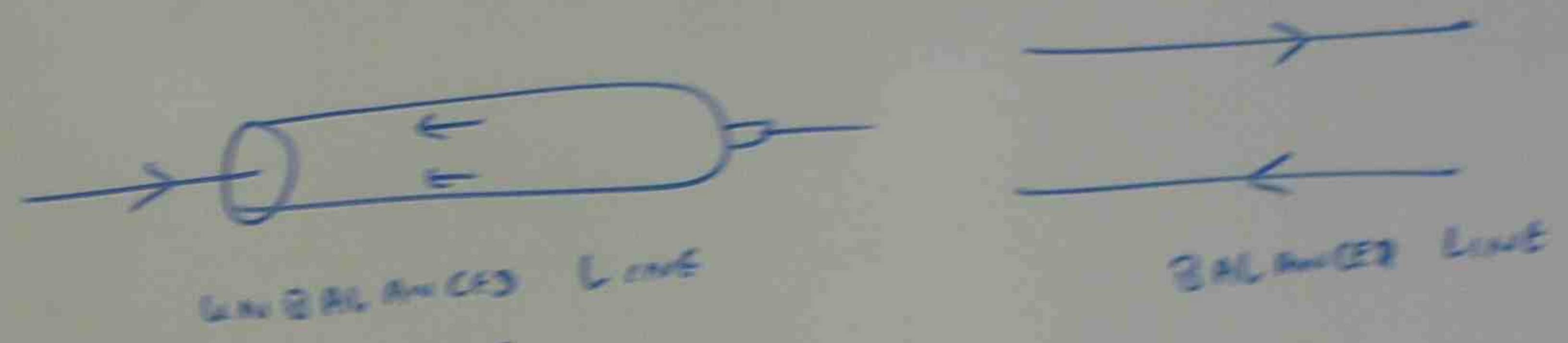
Q7 EXPLAIN TOUCH VOLTAGE,
STEP VOLTAGE, MESH VOLTAGE

Q8 WHAT IS FUNCTIONAL EARTH
AND PROTECTIVE EARTH?

Q037

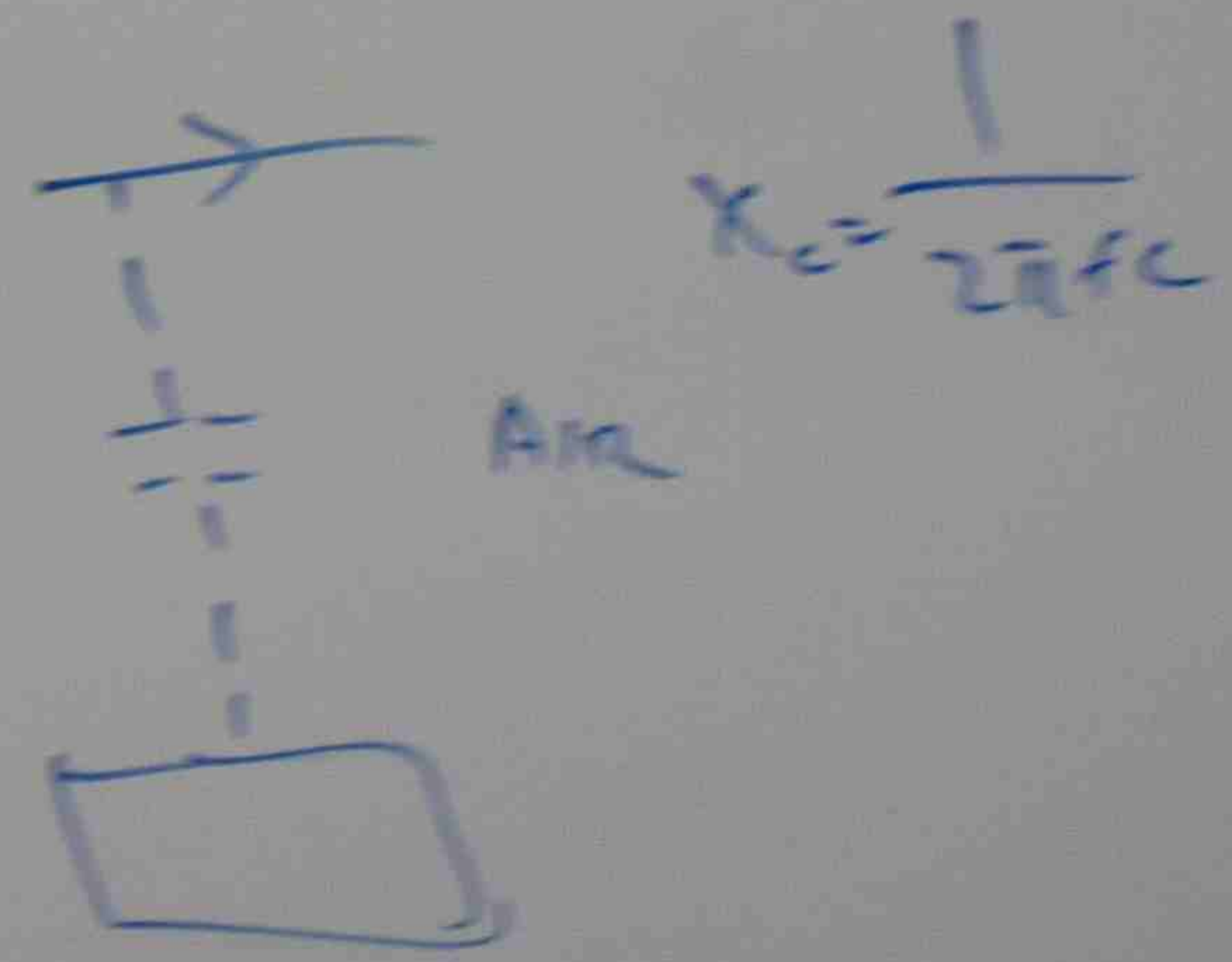
Coupling INTERFERENCE INTO ELECTRICAL SYSTEM

UNBALANCED LINE (CABLE) GENERATES INTERFERENCE



INTERFERENCE SIGNAL
PROTECTED BY SHIELDING

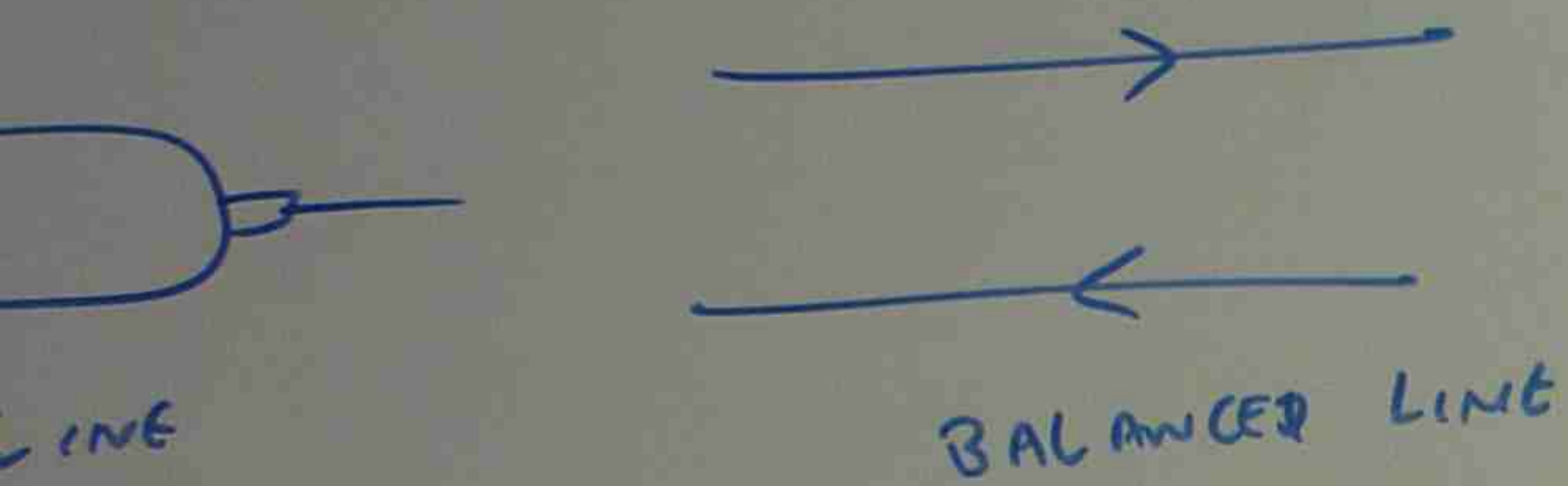
TRANSFER BY
COUPLING EFFECT
OF CAPACITOR



Coupling
Coupling
ONE CIR
MATCH
ELECTR
LIGHTN
COMPOS
META
SURGE
- APP
DEU
- TRAN
IN
- ISO
- POL
- UN

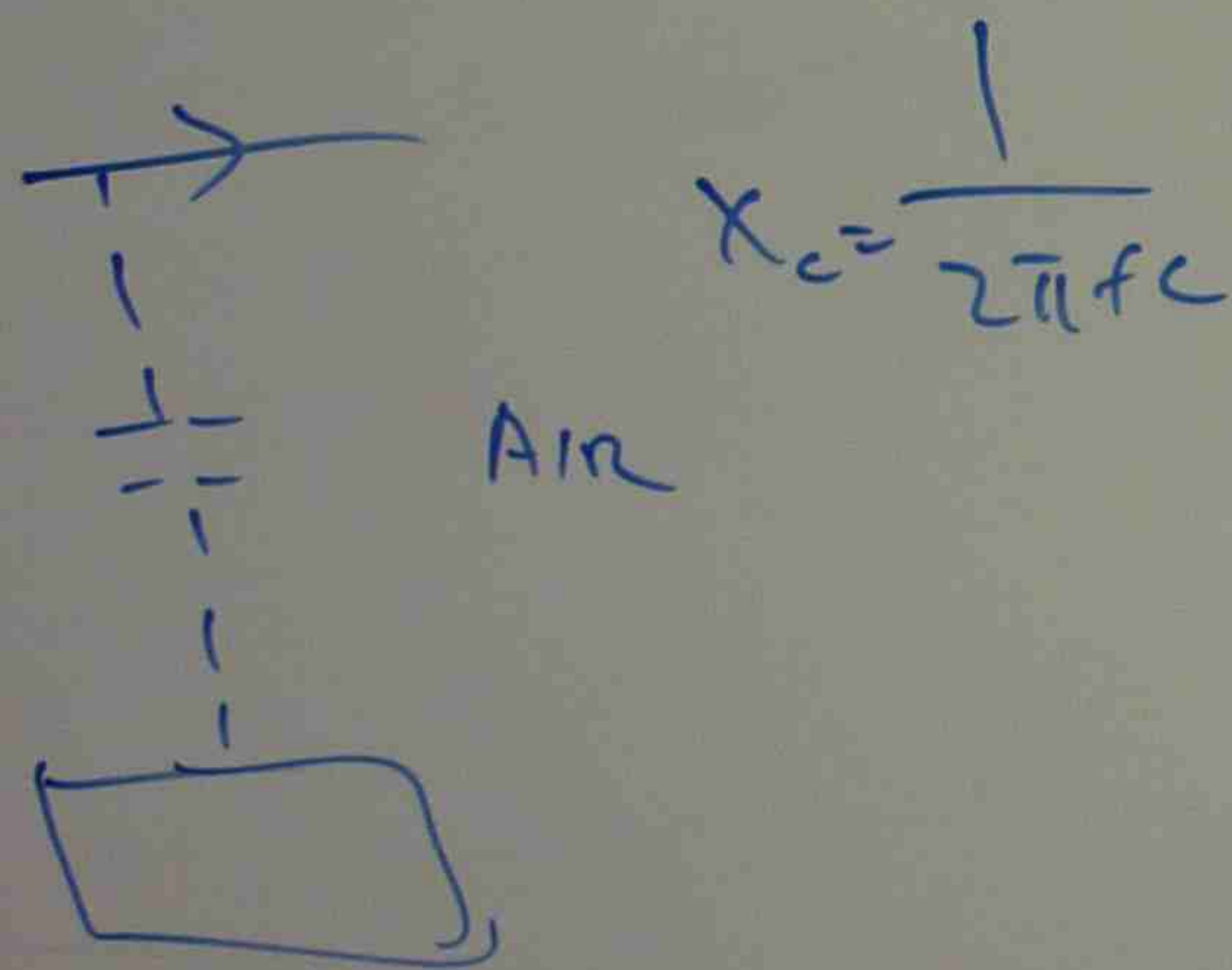
ANCE INTO ELECTRICAL SYSTEM

GENERATES INTERFERENCE



ERENCE SIGNAL

PROTECTED BY SHIELDING



$$X_c = \frac{1}{2\pi fC}$$

Air

Coupling

COUPLING IS TRANSFER OF ELECTRICAL ENERGY FROM ONE CIRCUIT SEGMENT TO ANOTHER. (IMPEDANCE MATCHING).

ELECTRICAL SHIELDING & SURGE PROTECTION

LIGHTNING PROTECTION

COMPOSES OF NETWORK OF LIGHTNING RODS, METAL CONDUCTORS, GROUND ELECTRODES

SURGE PROTECTOR

- APPLIANCE DESIGNED TO PROTECT ELECTRICAL DEVICES FROM VOLTAGE SPIKE.
- TRANSIENT VOLTAGE SURGE SUPPRESSORS ARE USED IN POWER SYSTEM TO PROTECT VOLTAGE SURGE.
- ISOLATION TRANSFORMER
- POWER CONDITIONERS
- UN INTERRUPTIBLE POWER SUPPLY

Q9

Q10

POOR POW

POOR POWER

- DEGRAD

- DECREASED

AND DIST

- POOR U

- INCREASE

HARMON

- HIGHER TH

- CAN CAUS

POOR POWER FACTOR

POOR POWER FACTOR HAS MANY DISADVANTAGES

- DEGRADED EFFICIENCY OF DISTRIBUTION POWER SYSTEM
- DECREASED CAPACITY OF TRANSMISSION, SUB TRANSMISSION AND DISTRIBUTION SYSTEM
- POOR VOLTAGE REGULATION
- INCREASED SYSTEM LOSSES.

IMPROVED BY

- CAPACITOR BANK
- SYNCHRONOUS MOTOR
- STATIC VAR CONTROL SYSTEM (SVC)

HARMONIC

- HIGHER THAN FUNDAMENTAL FREQUENCY
- CAN CAUSE
 - TEMPERATURE RISE ABOVE RATED TEMPERATURE
 - VIBRATION WITH IN MACHINE
 - DECREASED LIFE TIME DUE TO INTERMITTENT OPERATION.
 - HEATING OF EQUIPMENTS & THERMAL AGING

HARMONIC DISTORTION DEPENDS ON

LEVEL of HARMONIC GENERATION
SYSTEM FREQUENCY RESPONSE CHARACTERISTICS

TOTAL HARMONIC DISTORTION NEEDS TO BE CALCULATED.

- HARMONIC CAN BE CREATED IN TRANSFORMER
- FILTER WILL NEED TO BE USED.

Q9 WHAT IS COUPLING?

Q10 EXPLAIN ELECTRICAL SHIELDING & SURGE PROTECTION

Q11 WHAT ARE THE DISADVANTAGES OF POOR POWER FACTOR
& HOW CAN IT BE IMPROVED?

Q12 WHAT ARE THE DISADVANTAGES OF HARMONIC, HOW IS THE SYSTEM
DEPENDENT ON SELF PROTECTION FOR HARMONIC.
WHICH METHODS ARE REQUIRED TO BE USED FOR HARMONIC
PROTECTION?

Q13 HOW CAN ELECTRICAL INTERFERENCE OCCUR? SKETCH THE DIAGRAM.

SITE

THE

①

②

③

④

Q7

6039

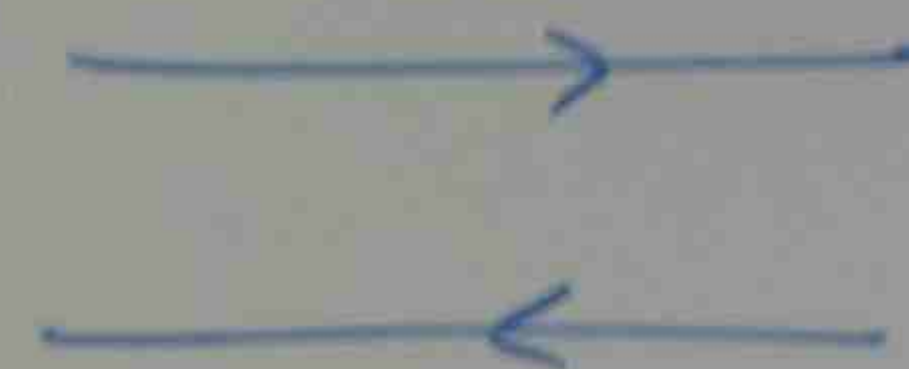
COUPLING INTERFERENCE INTO ELECTRICAL SYSTEM

UNBALANCED LINE / CABLE GENERATES INTERFERENCE

Q13



UNBALANCED LINE

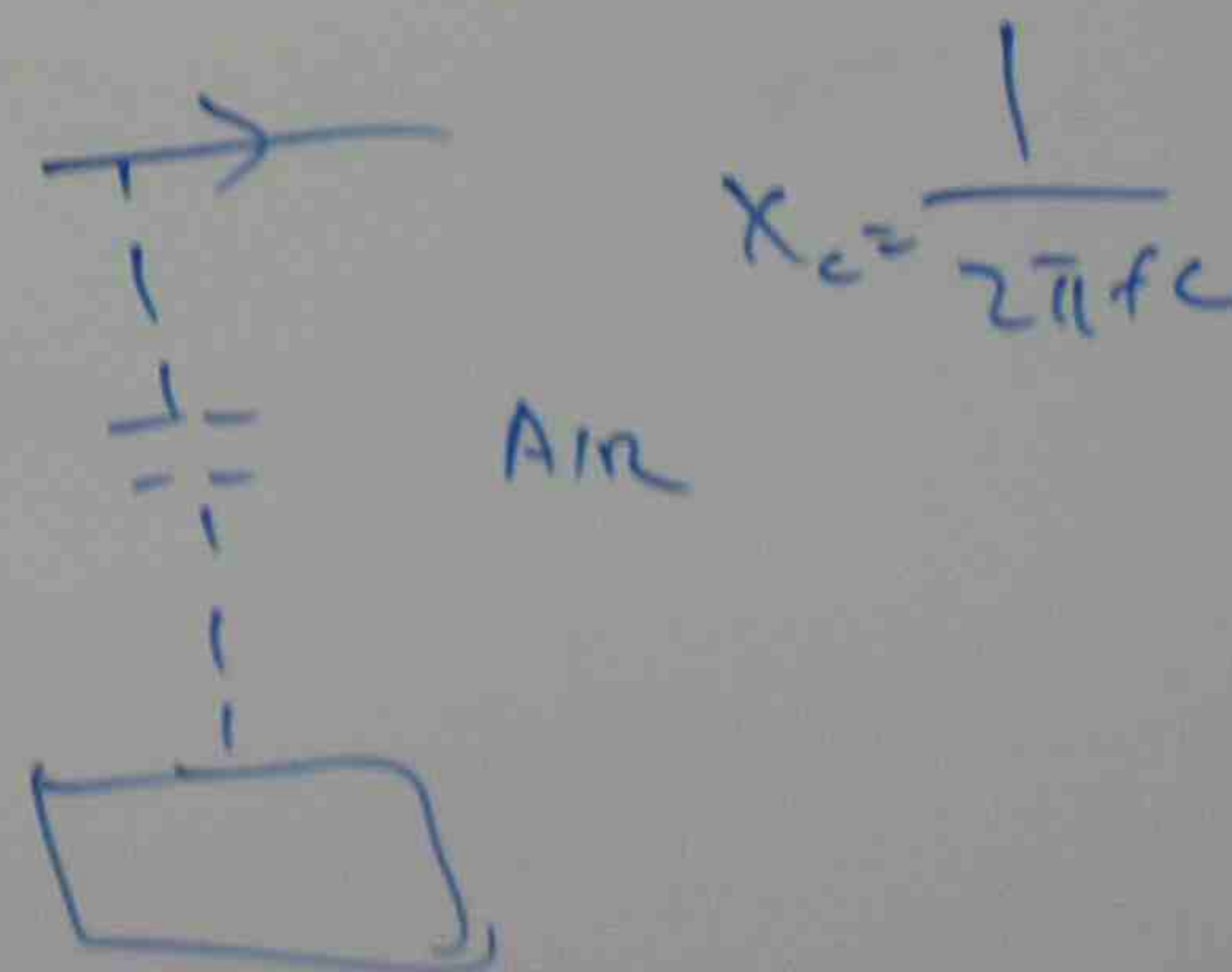


BALANCED LINE

INTERFERENCE SIGNAL

PROTECTED BY SHIELDING

TRANSFER BY
COUPLING EFFECT
OF CAPACITOR



Coupling

coupling is T
ONE CIRCUIT
MATCHING).

ELECTRICAL S

LIGHTNING P

composes of
METAL CON

SURGE PROT

- APPLIANCE
DEVICES f

- TRANSIENT
IN POWER

- ISOLATION

- POWER CON

- UNINTO