

**Arrange circuits, control
and
protection
for
general electrical installations**

Week 2: Fault Loop Impedance

A QUALITY VOCATIONAL ELECTRICAL TRAINING COURSE
PROVIDED BY: **GLOBAL ENERGY TRAINING SOLUTIONS**

All writing in BLUE is examinable

**All writing in RED
is
NOT examinable.**

The cable selection process

Glossary:

MD = Maximum Demand

CB = Circuit Breaker

CCC = Current Carrying
Capacity

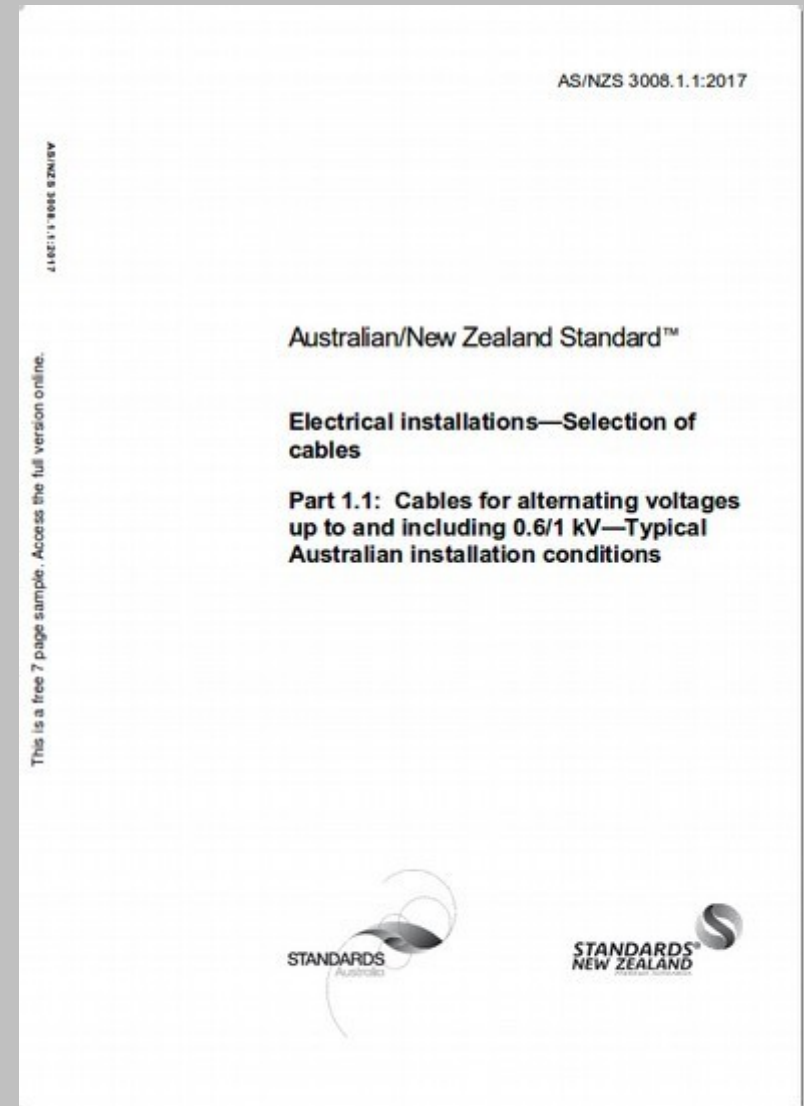
VD = Voltage Drop

FLI = Fault Loop Impedance

PFC = Prospective Fault Current

SCTR = Short Circuit

Temperature Rise



- 1) Calculate MD (AS/NZS 3000)
- Consumer mains (Table C1, C2, C3)
 - Sub mains (Table C1, C2, C3)
 - Final sub circuits (Table C4, C8)

- 2) Select Circuit Breaker
(Standard sizes Table 8.1 AS/NZS 3000)

$$I_B \leq I_N \leq I_Z$$
$$MD \leq CB \leq CCC$$

2.5.3.1 AS/NZS 3000

- 3) Select cable based on Current Carrying Capacity
(Table C5 and C6 AS/NZS 3000, Section 3 AS/NZS 3008)

- 4) Check Voltage Drop
(3.6, Table C7 AS/NZS 3000, Section 5 AS/NZS 3008)

- 5) Check Fault-Loop Impedance
(5.7, Appendix B AS/NZS 3000)

6) Calculate Prospective Fault Current
(2.5.4 AS/NZS 3000) However no guidance is offered in
AS/NZS 3000

7) Check Short Circuit Temperature Rise
(2.5.4 and Section 5 AS/NZS 3008)

This course covers FLI, SCTR and PFC, however these are only topics inside the much greater cable selection process.

Fault-Loop Impedance

What you need to know about Fault-Loop Impedance

- 1) What is it?
 - Describe the loop
 - Why it is an issue

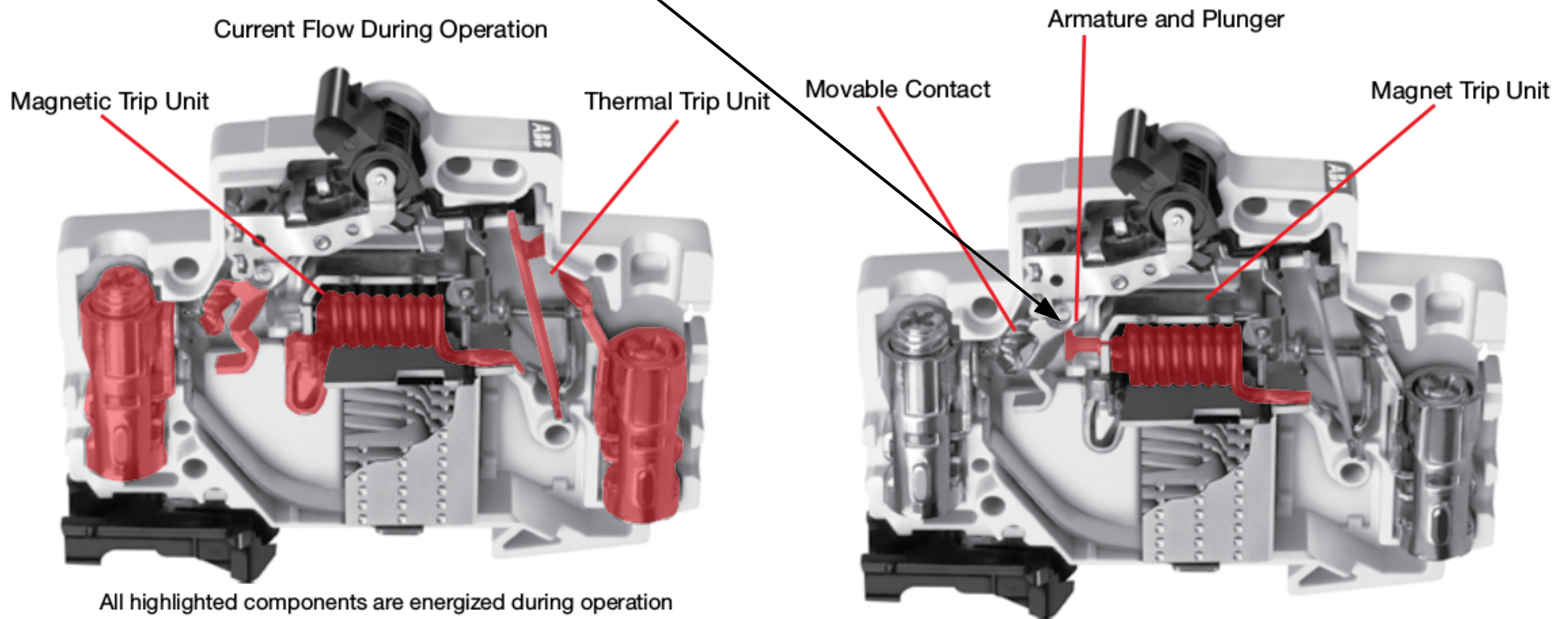
 - 2) How to select cables so that maximum lengths are not exceeded:
 - L_{max}
 - Table B1

 - 3) How to test it:
 - Table 8.1 (live)
 - Table 8.2 (dead)
- (Z_{max})

Circuit breakers

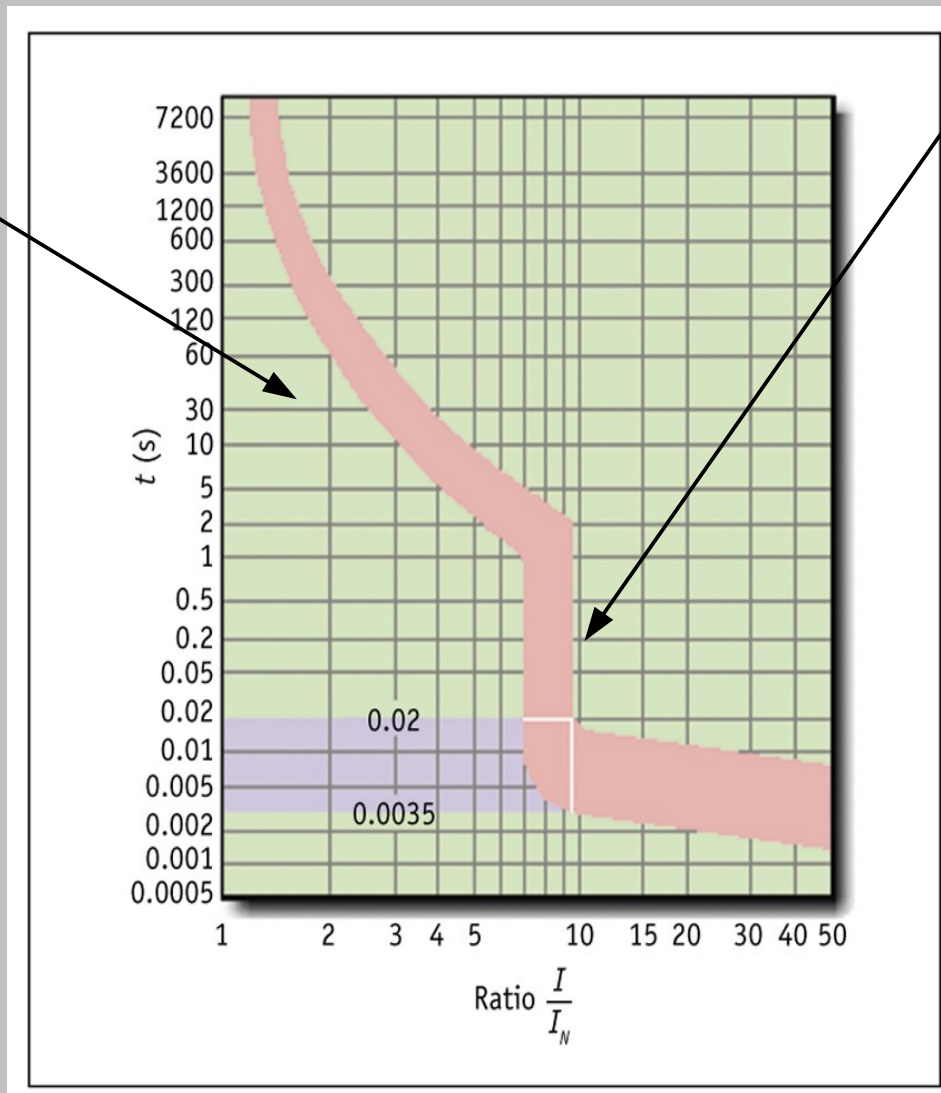
If not enough current flows this Solenoid wont trip during a short.

We calculate this using another application of Ohms law.



Thermal trip
(Bi-metal Strip)
(Conventional trip
Time)

$$(I_B \leq I_N \leq I_Z)$$



Magnetic trip
(Solenoid)
(Instantaneous
Trip)
(Fault-Loop
Impedance)

Not all circuit breakers trip the same

Type B – 4 x overload $20A \times 4 = 80A$ to trip instantly

Type C – 7.5 x overload $20A \times 7.5 = 150A$ to trip instantly

Type D – 12.5 x overload $20A \times 12.5 = 250A$ to trip instantly
(B4.5 AS/NZS 3000)

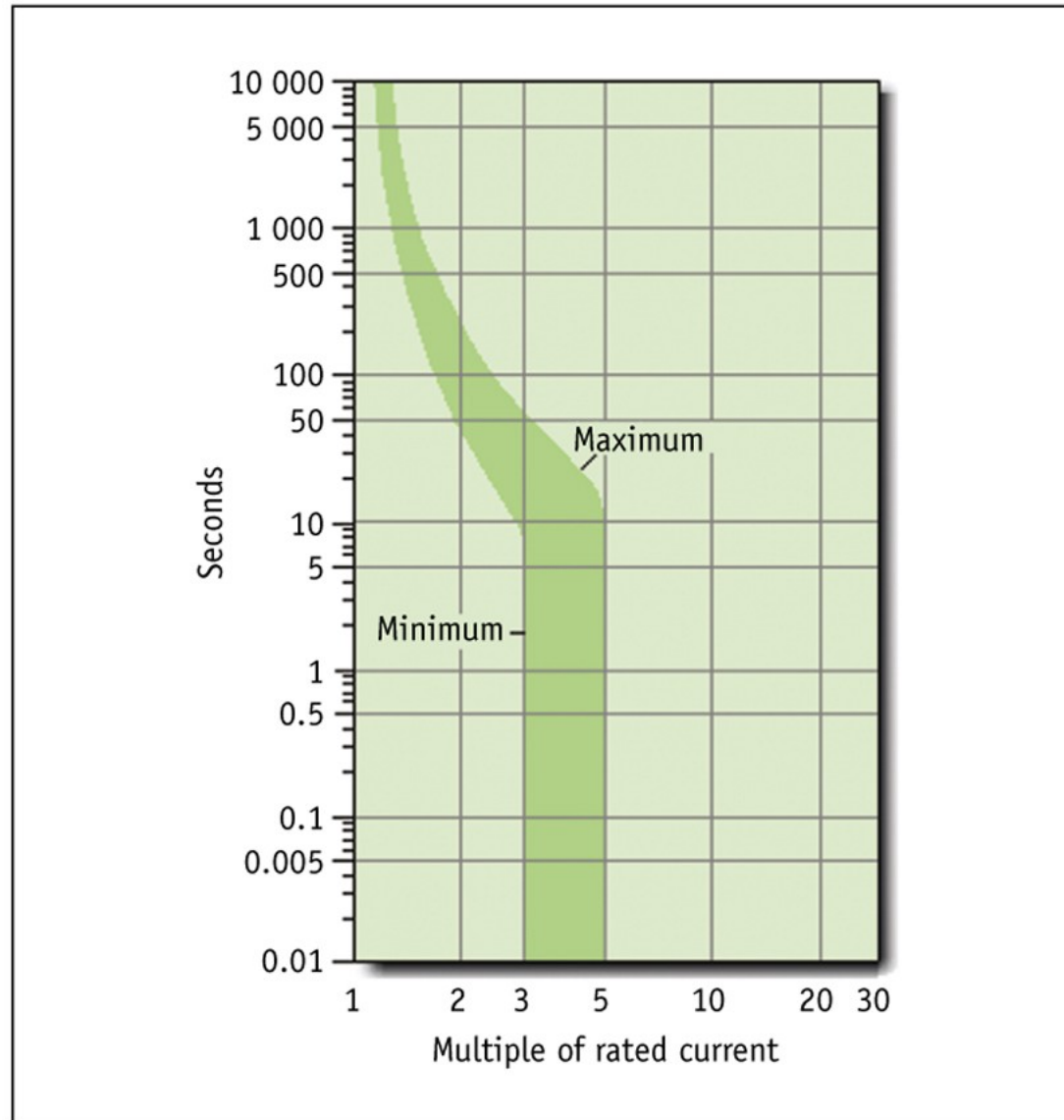
Type B – Where a fast trip time is required
or to protect a sensitive load

Type C – All common CB's

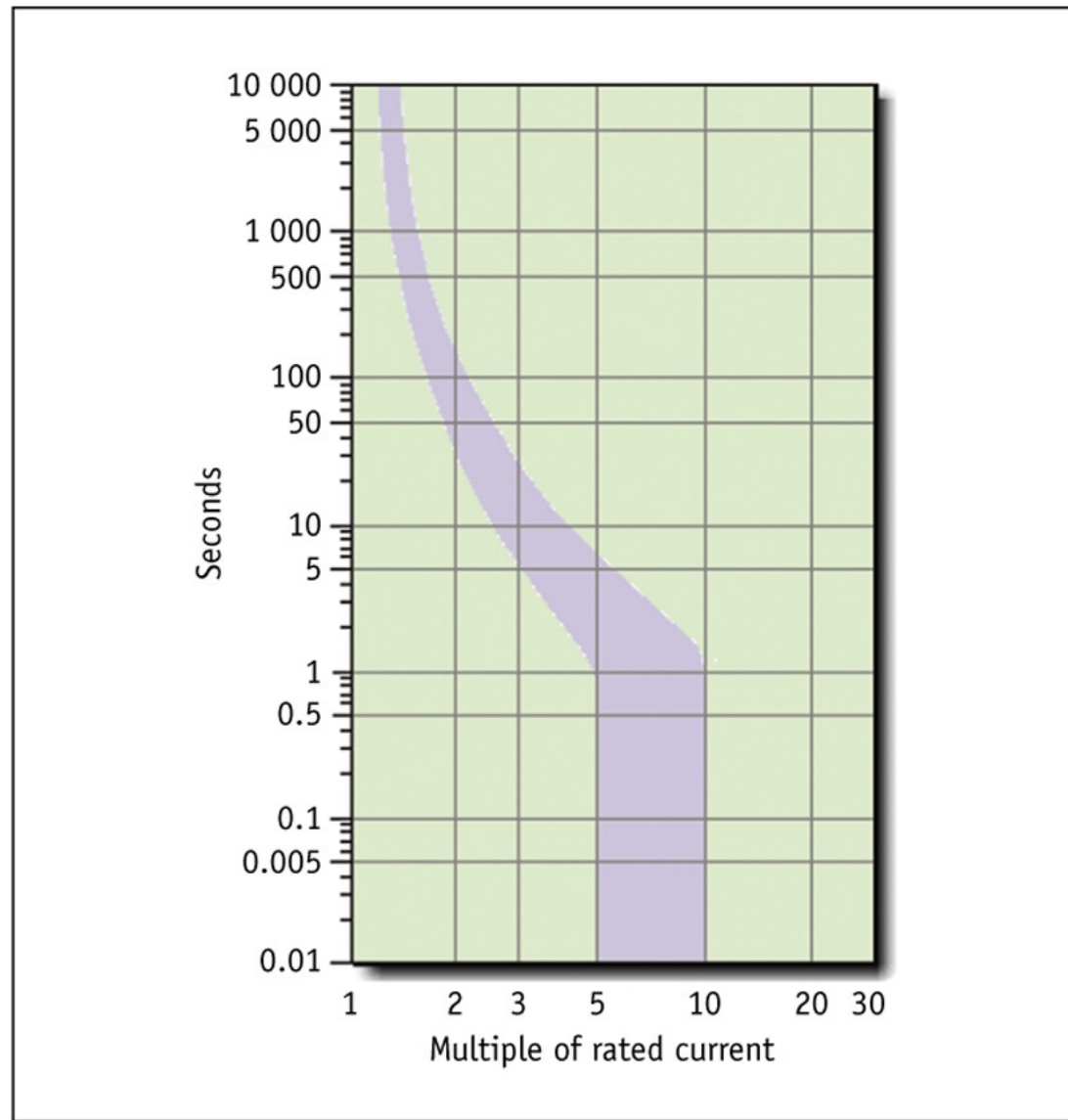
Type D – Used for high start up current
applications such as Direct On Line (DOL)
motors

The letter is indicated on CB's C20
= Type C 20A CB

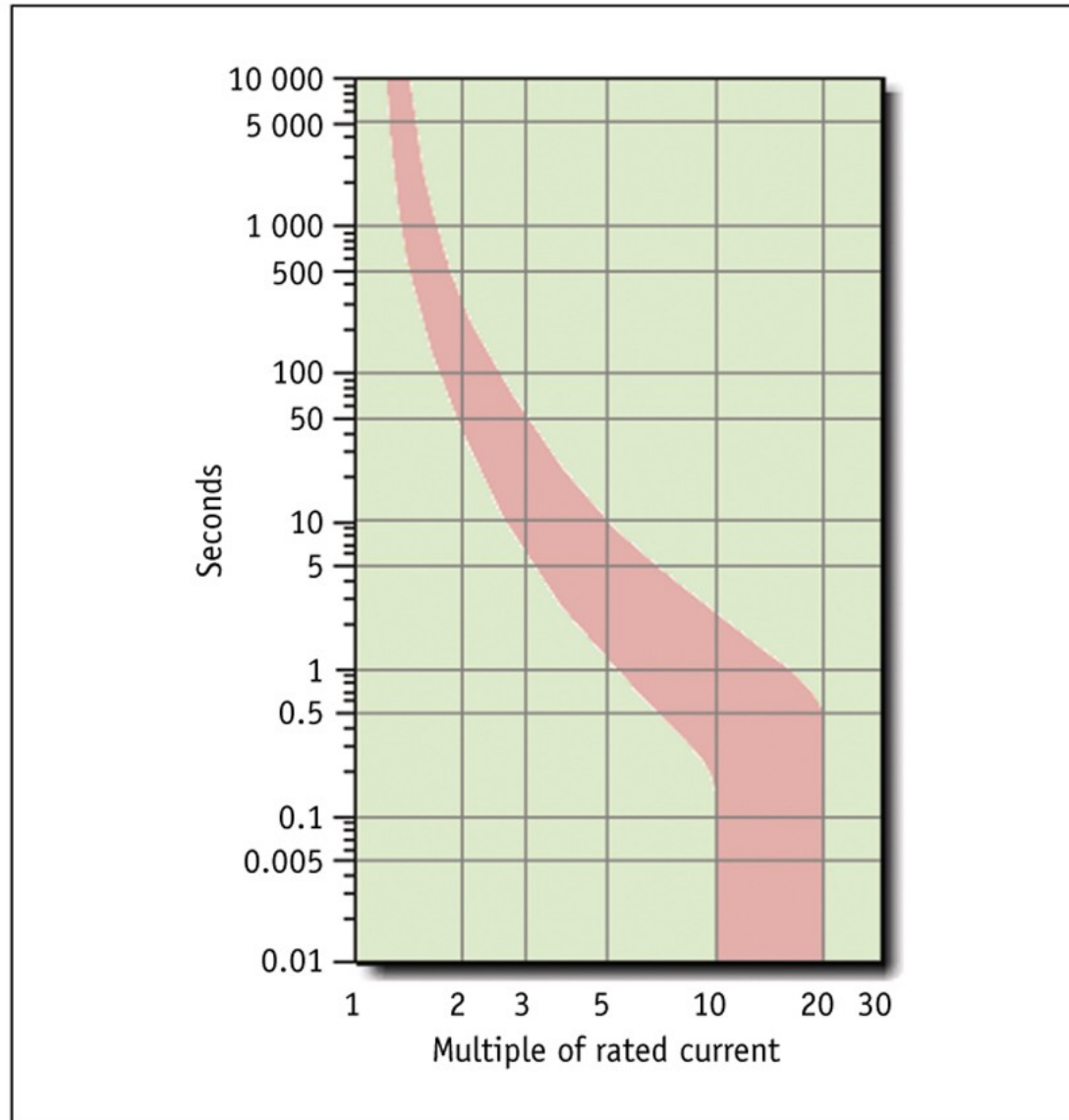




Type B: 4 x



Type C: 7.5 x



Type D: 12.5 x

Glossary:

FLI = Fault-Loop Impedance

TX = Transformer

CM = Consumer Main

MSB = Main Switch Board

SM = Sub-Main

DB = Distribution Board

FSC = Final Sub-Circuit

Load = Load

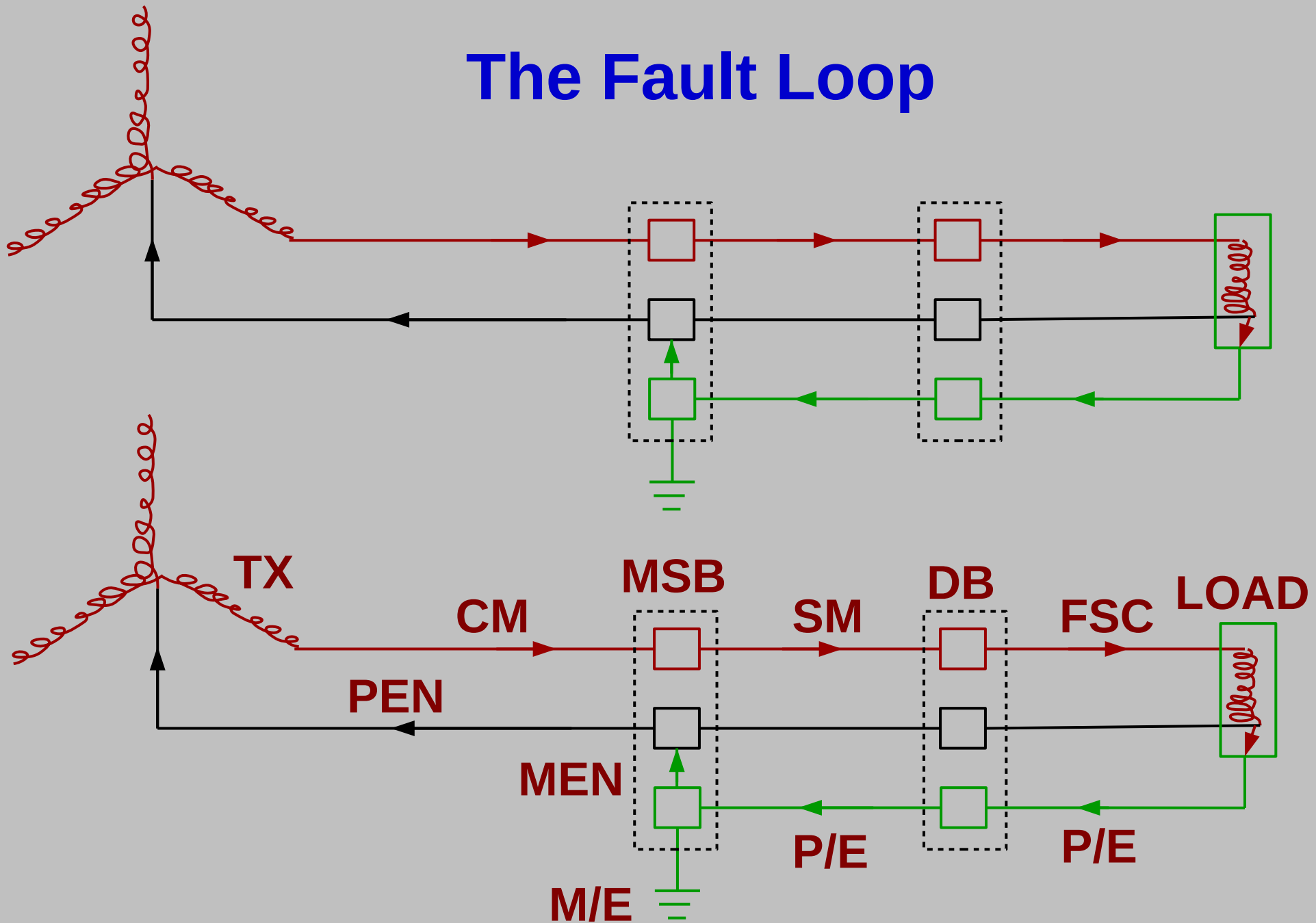
P/E = Protective Earth

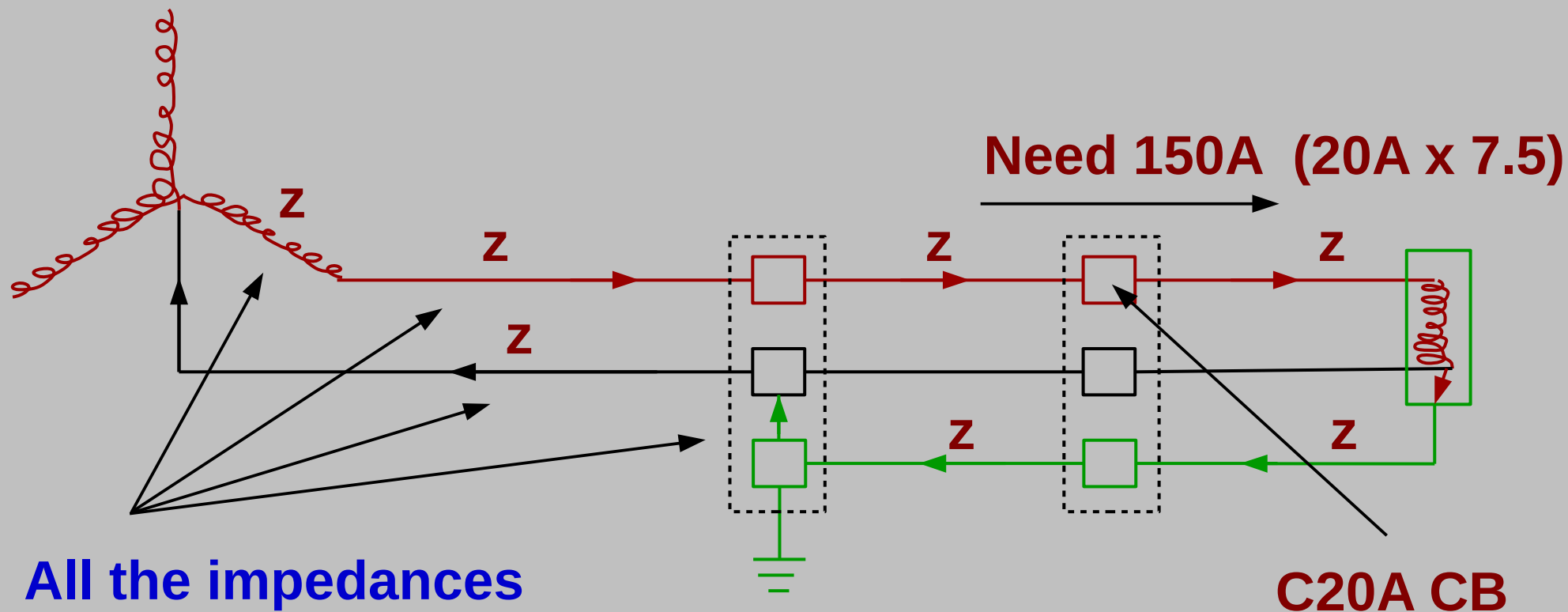
M/E = Main Earth

MEN = Main Earth Neutral

PEN = Protective Earth Neutral

The Fault Loop

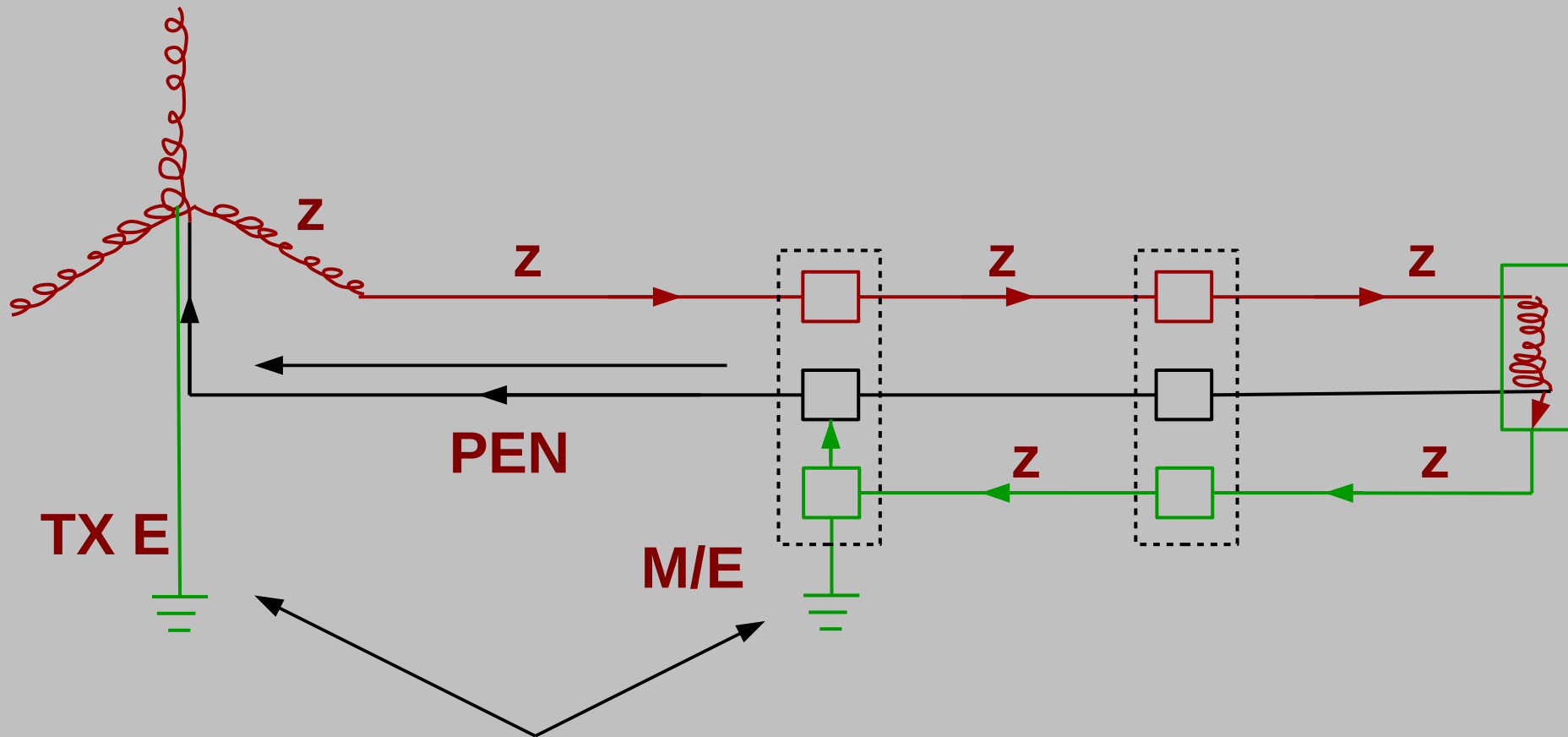




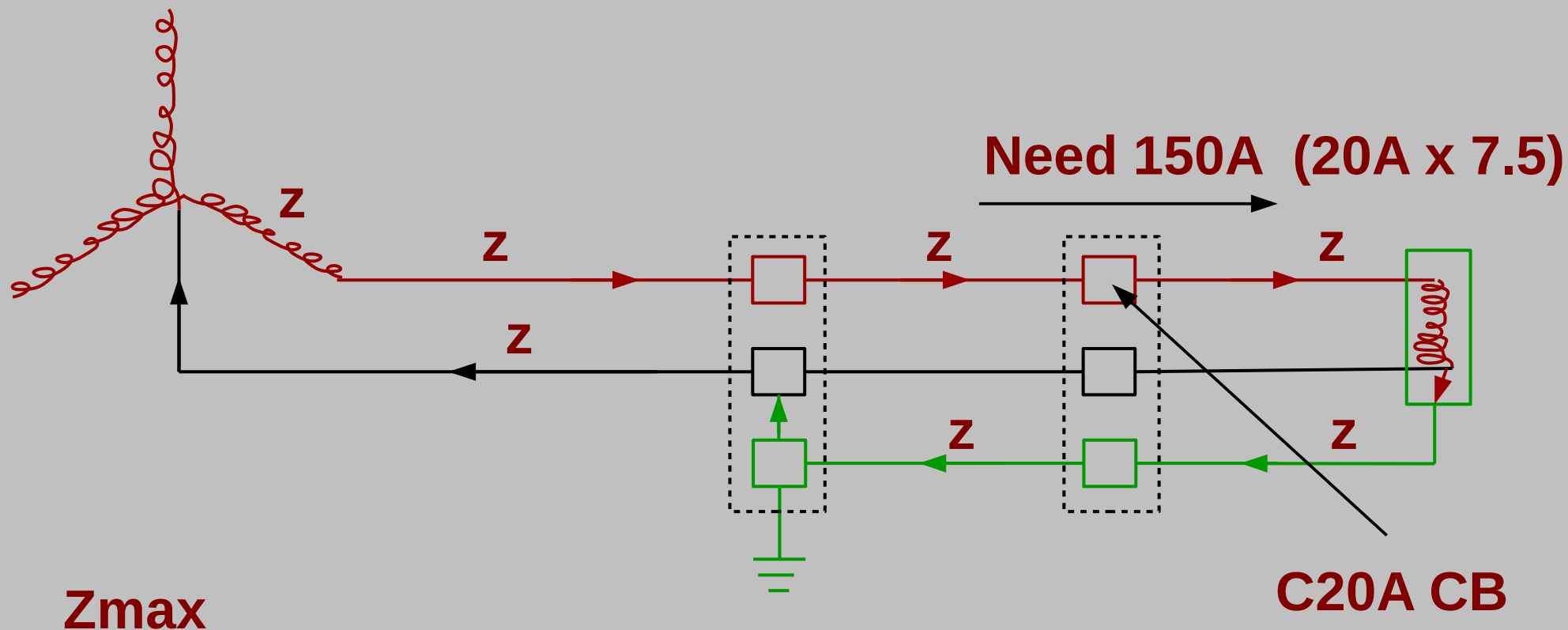
All the impedances added together makes the Fault-Loop Impedance

5.7.4 AS/NZS 3000 gives the formula: $Z_s \times I_a \leq U_0 = Z_s = \frac{U_0}{I_a}$ or $(Z_{max} = \frac{V}{I_a})$

I_a – Is the current required to trip the circuit breaker. (I_a is Amps rated on the circuit breaker times the class)

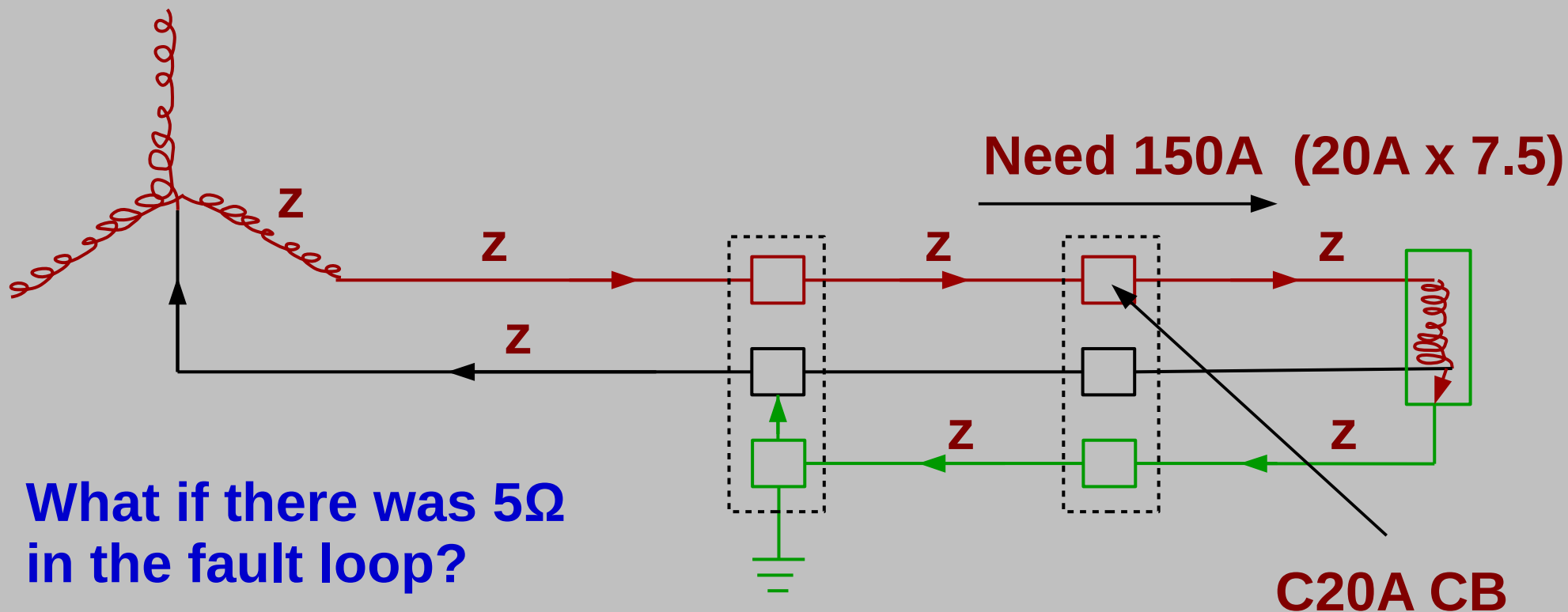


Barely any current runs through the ground as the impedance is much higher than the PEN conductor



$$Z_{max} = \frac{V}{I_a} = \frac{230}{(7.5 \times 20)} = 1.533 \Omega$$

Now check this against Table 8.1



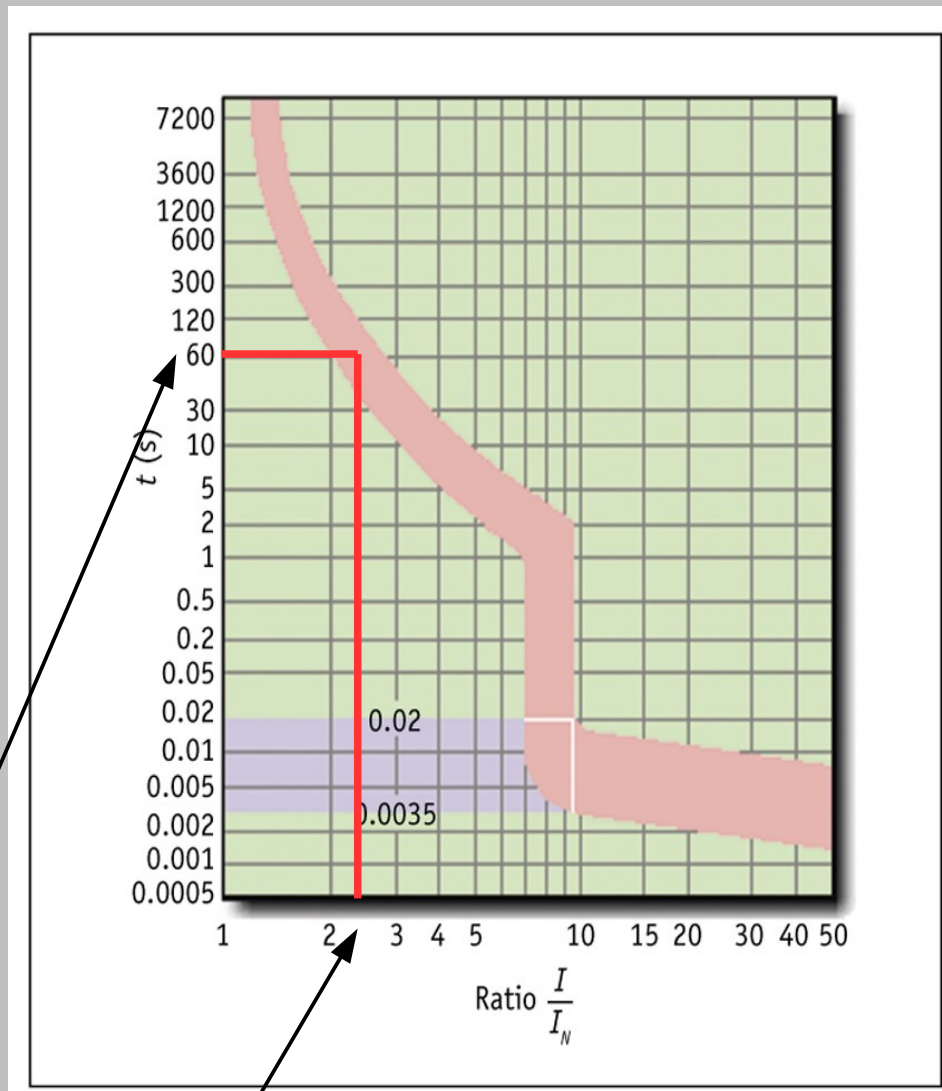
What if there was 5Ω in the fault loop?

$$\text{Transposed} = I_a = \frac{V}{Z} = \frac{230 \text{ V}}{5 \Omega} = 46 \text{ A}$$

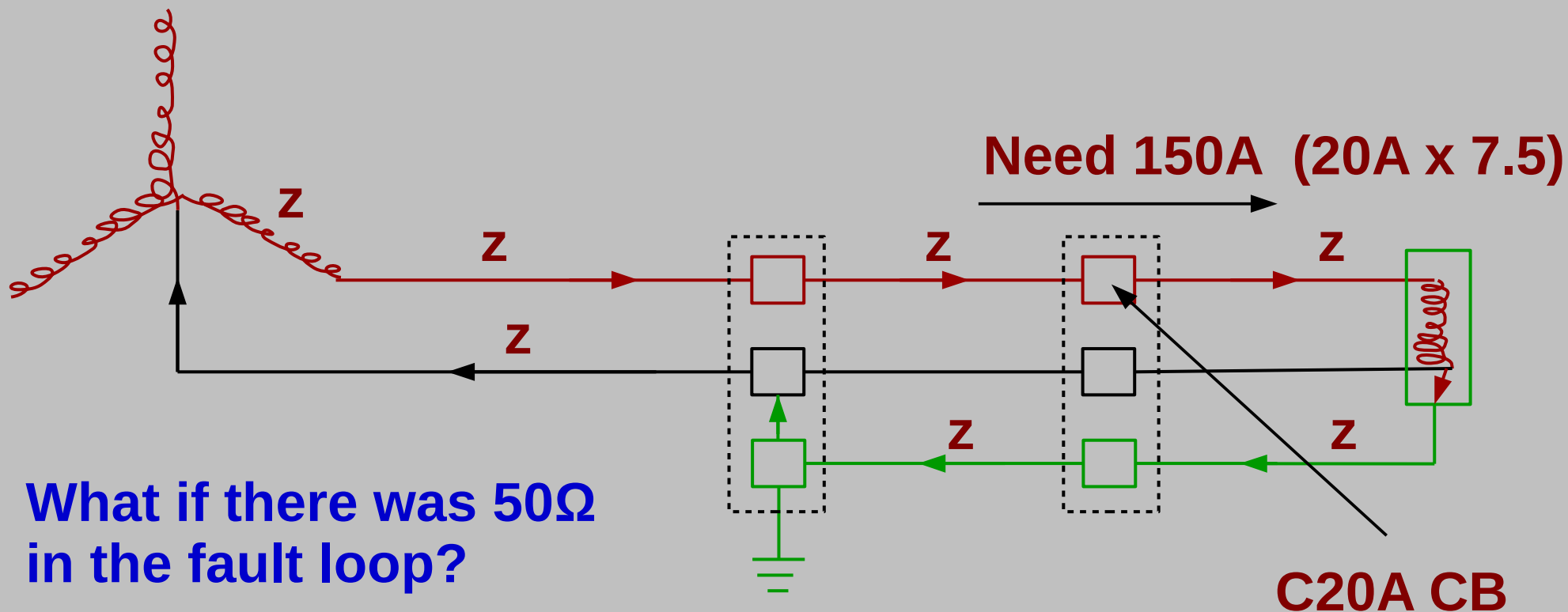
$$\frac{46 \text{ A}}{20 \text{ A}} = 2.3 \times \text{Overload}$$

How long will it take to trip the CB

Not fast enough (60 seconds) we need 7.5 x overload to turn the power off in 0.4 seconds max.
5.7.2 AS/NZS 3000



2.3 x Overload



What if there was 50Ω in the fault loop?

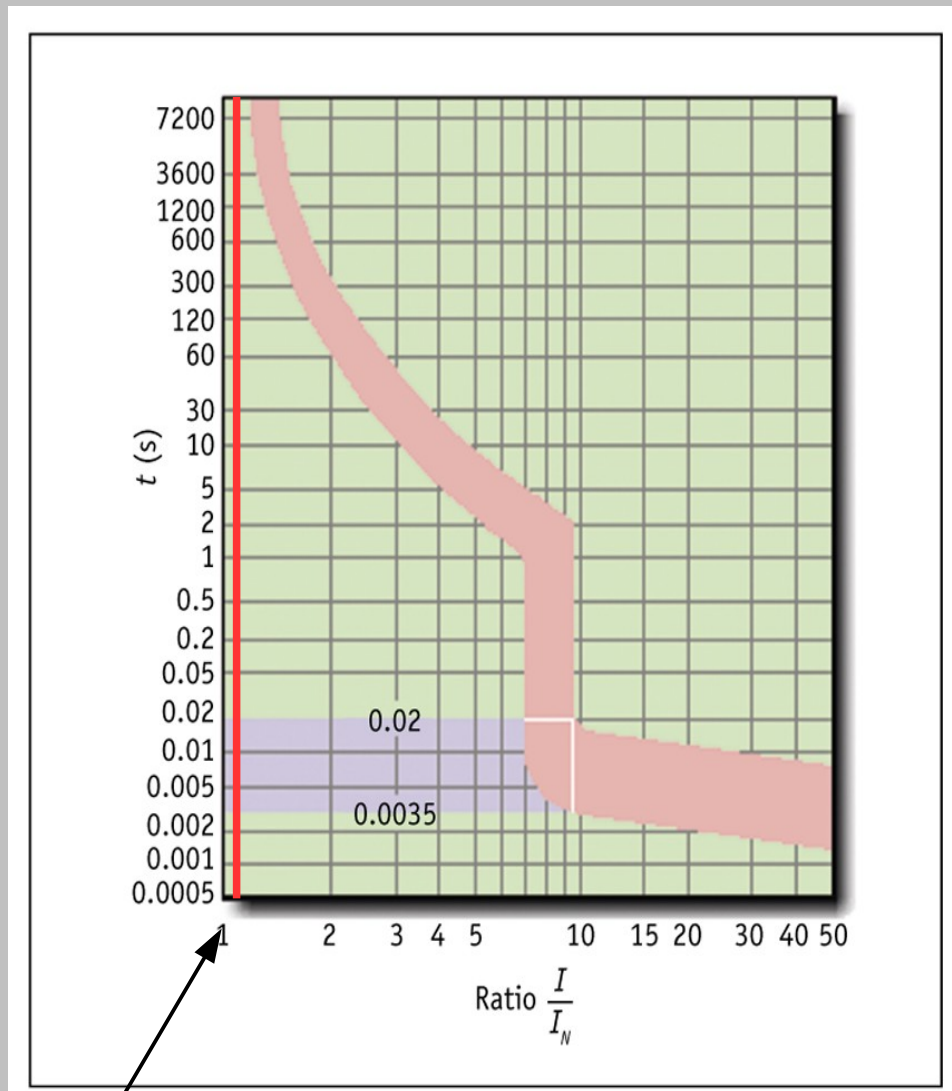
$$I_a = \frac{V}{Z} = \frac{230 \text{ V}}{50 \Omega} = 4.6 \text{ A}$$

$4.6 \text{ A} = 0 \times \text{Overload}$

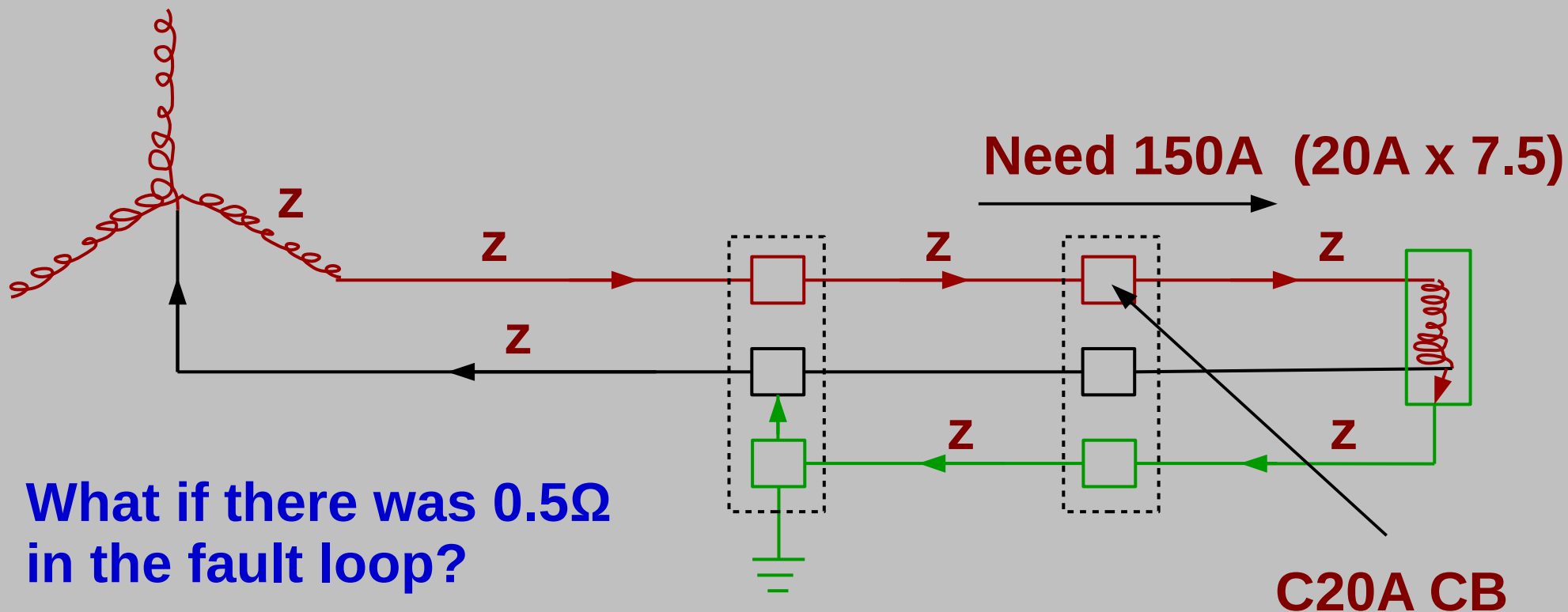
How long will it take to trip the CB

A circuit breaker may never trip with a 50Ω Fault-Loop

Don't leave the MEN out or you will render your circuit breakers useless!



0 x Overload



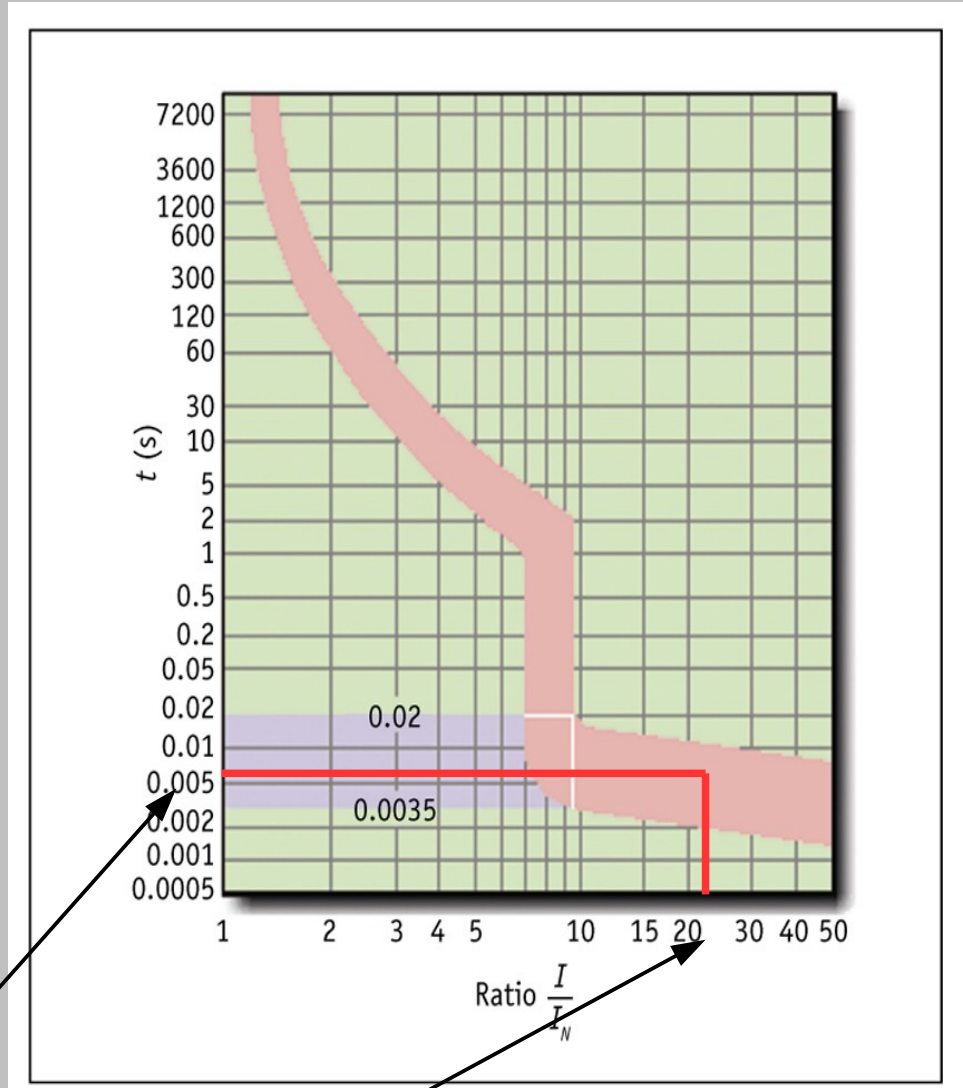
What if there was 0.5Ω in the fault loop?

$$I_a = \frac{V}{Z} = \frac{230 \text{ V}}{0.5 \Omega} = 460 \text{ A}$$

$$\frac{460 \text{ A}}{20 \text{ A}} = 23 \times \text{Overload}$$

How long will it take to trip the CB

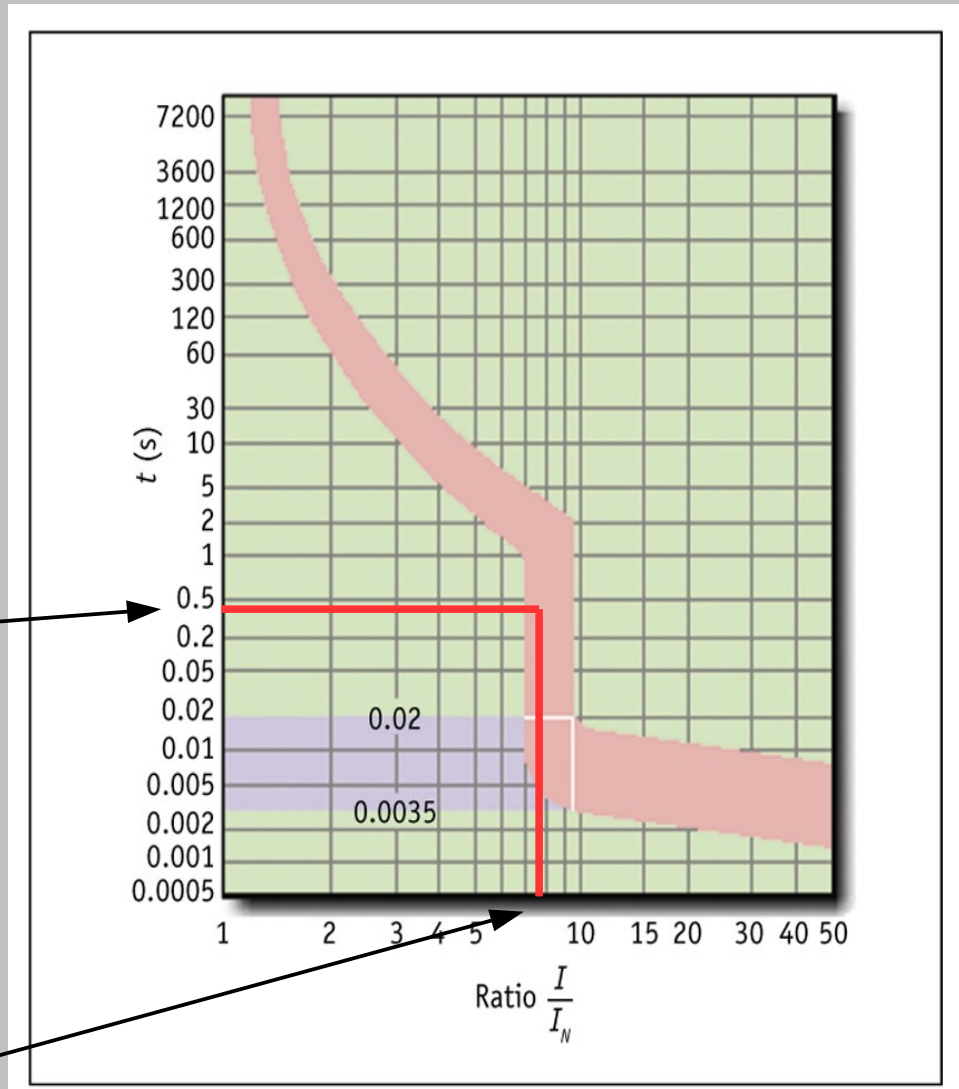
Easily faster than the minimum disconnection time or 0.4 seconds

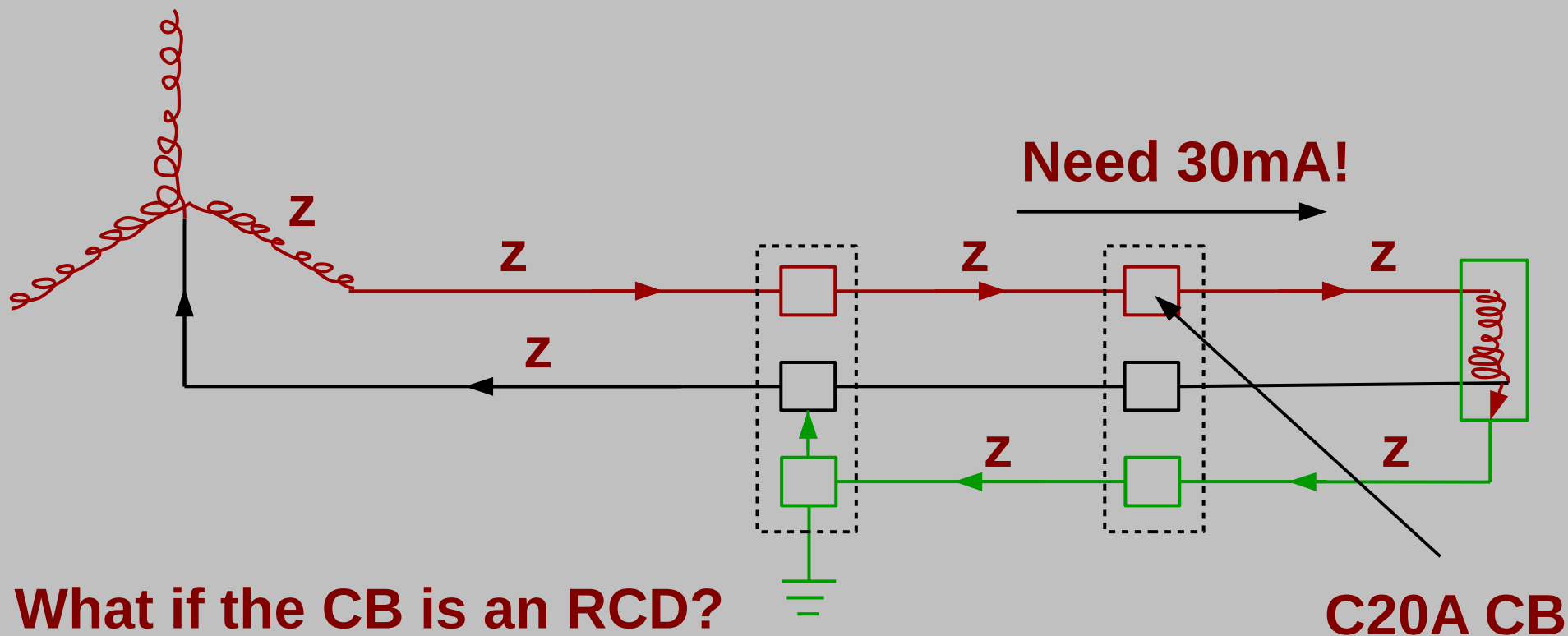


23 x Overload

7.5 x overload is the minimum current required to cause automatic disconnection of supply, (in 0.4 s) therefore 1.53Ω is the maximum fault-loop impedance for a C20A CB

$$Z_{\max} = \frac{V}{I_a} = \frac{230}{(7.5 \times 20)} = 1.533 \Omega$$

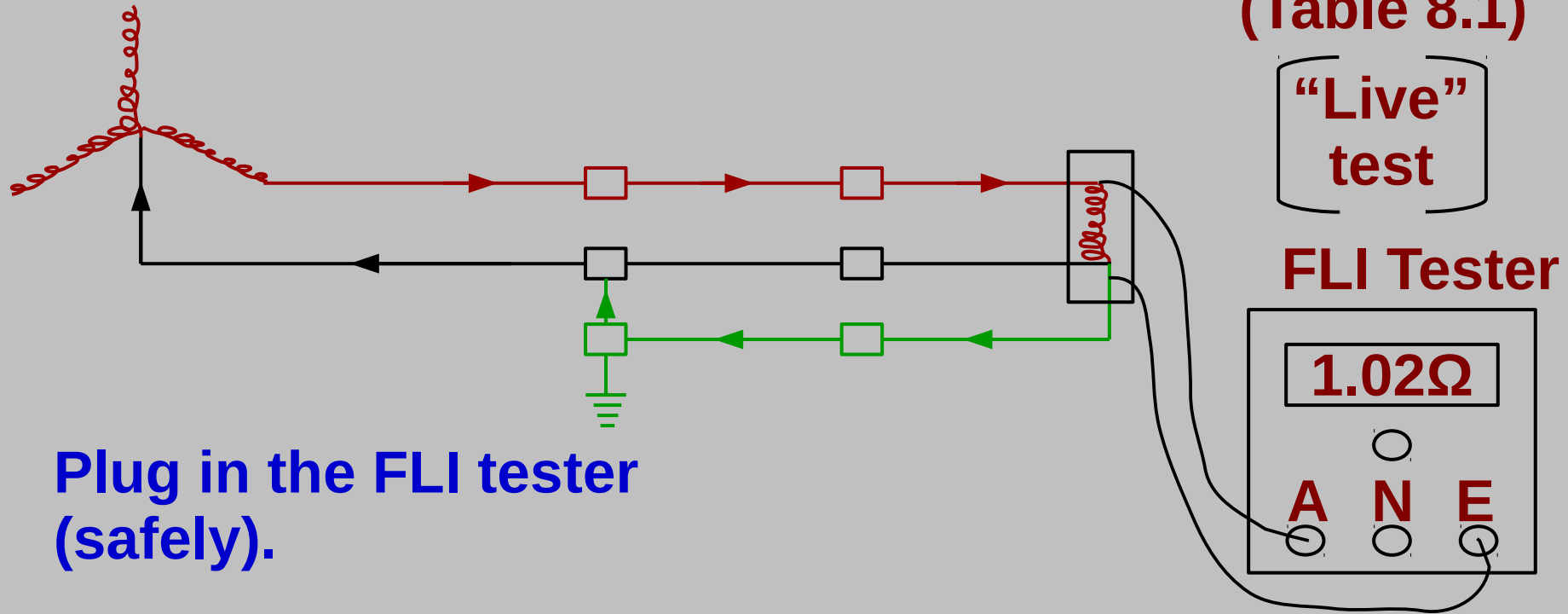




$$RCD = \frac{230 \text{ V}}{30 \text{ mA}} = 7667 \Omega$$

You can have almost 8kΩ in the fault loop and it will still trip (if the RCD is faulty, we are back to needing 150A)

Live testing

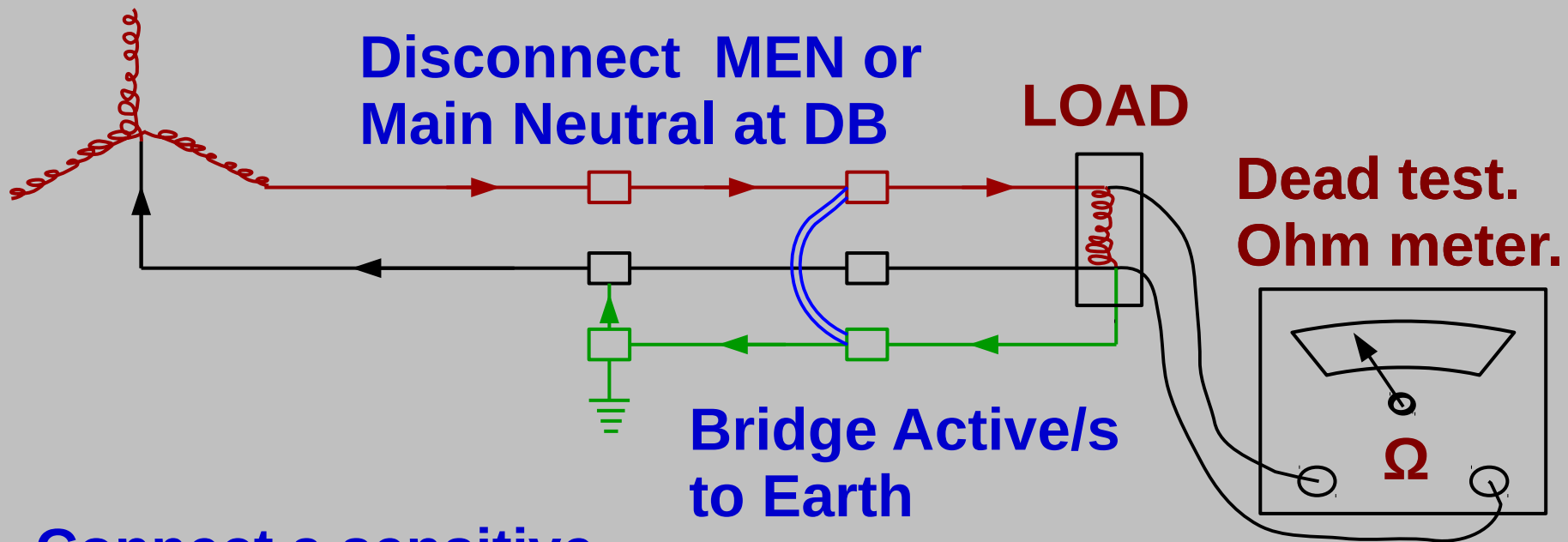


Plug in the FLI tester (safely).

Press the test button.

The value must be less than those in table 8.1 (Z_{max} for live test)

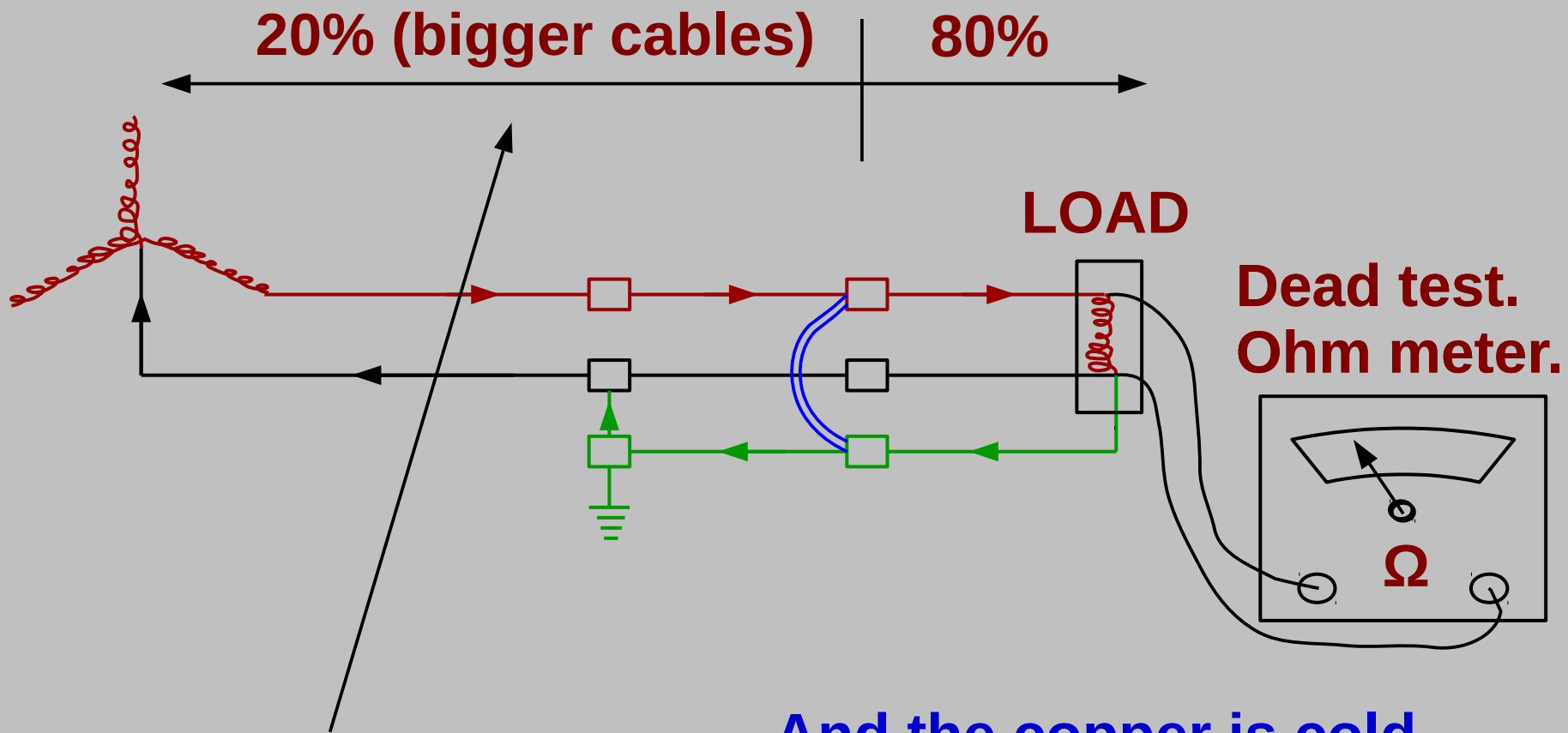
Dead testing



Connect a sensitive Ohm meter

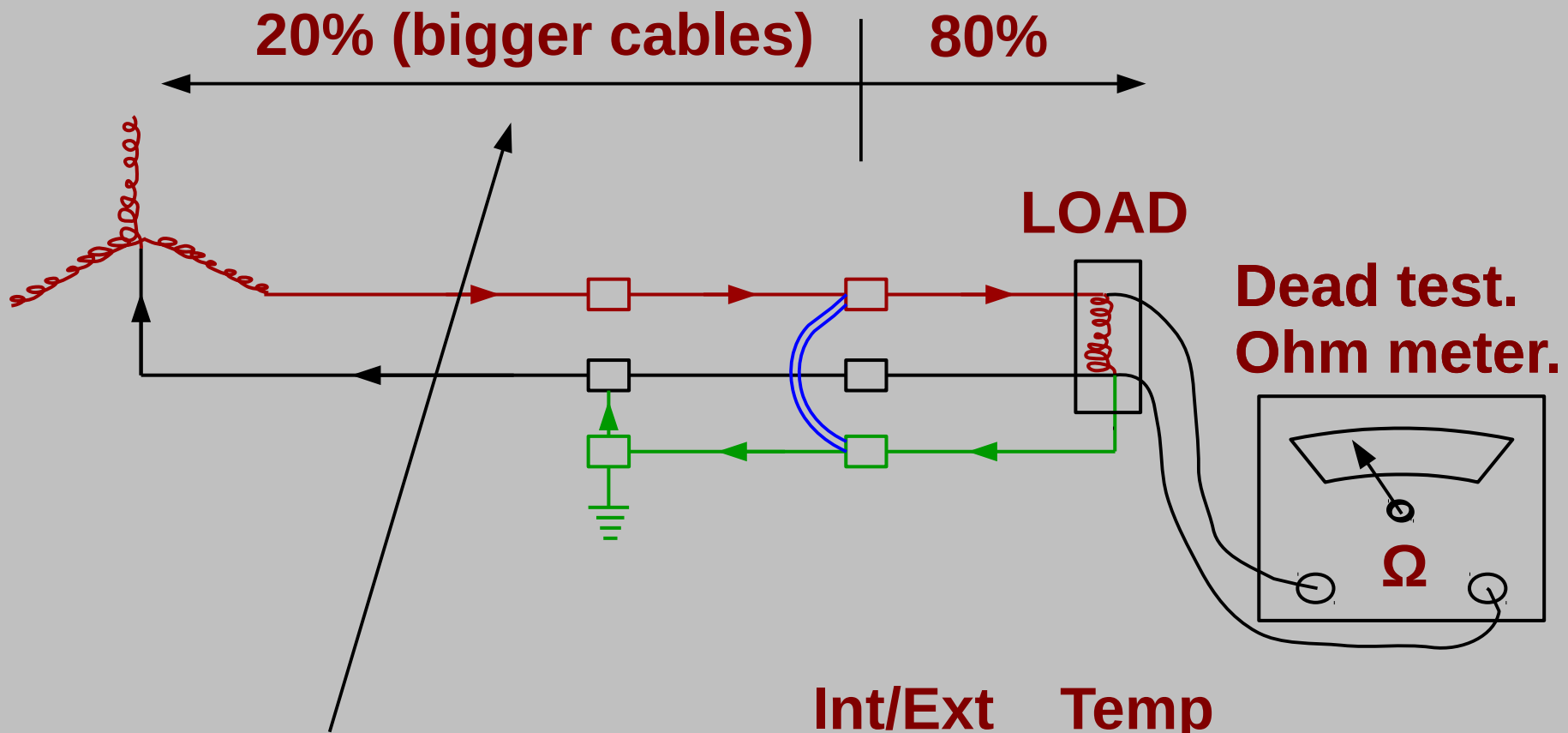
The value must be less than those in table 8.2 (Z_{max} for dead test)

A method accepted by AS/NZS 3000 that does not require an expensive meter



However this method does not test 20% of the circuit

And the copper is cold when tested and could have a higher resistance when operating at 75°



Therefore we use the following modified formula:

$$Z_{max} = \frac{V}{I_a} \times \overset{\text{Int/Ext}}{0.8} \times \overset{\text{Temp}}{0.8}$$

$$0.8 \times 0.8 = 0.64$$

$$Z_{\max} = \frac{V}{I_a} \times 0.64 = \frac{230}{(20 \times 7.5)} = 0.98 \Omega$$

**Now check this against Table 8.2 (R_{phe})
(Resistance Phase to Earth)**

Max Circuit length

(So as not to have FLI issues)

Lmax – Maximum length

B5.2.2 AS/NZS 3000

$$L_{\max} = \frac{0.8 \times U_o \times S_{\text{ph}} \times S_{\text{pe}}}{I_a \times \rho \times (S_{\text{ph}} + S_{\text{pe}})}$$

Use Table B1 for most cases

U_o – Nominal phase volts (230V)

S_{ph} – Cross section area of the active conductor in mm^2

S_{pe} – Cross section area of the protective Earthing in mm^2

I_a – Trip setting x Rating of Circuit Breaker (e.g. 20 x 7.5)

ρ – Resistivity at normal working temperature in $\Omega\text{-mm}^2/\text{m}$

Cu – 0.0225 Ω

Al – 0.036 Ω

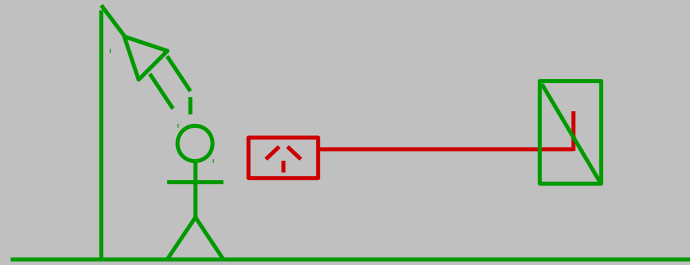
What is the max length of cable protected by a C20A CB with a 2.5mm Active and a 2.5mm Earth

$$L_{\max} = \frac{0.8 \times U_o \times S_{\text{ph}} \times S_{\text{pe}}}{I_a \times \rho \times (S_{\text{ph}} + S_{\text{pe}})}$$

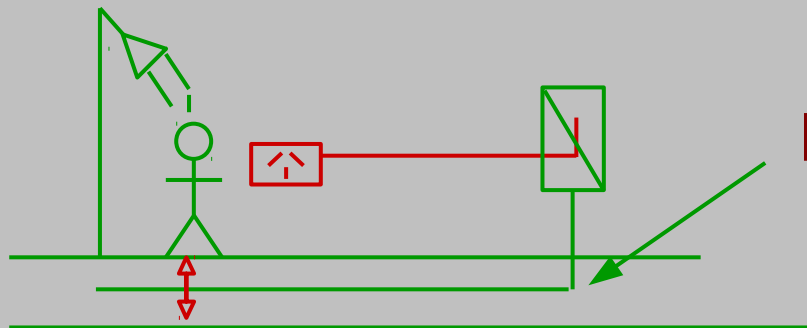
$$\begin{aligned} L_{\max} &= \frac{0.8 \times 230 \times 2.5 \times 2.5}{7.5 \times 20 \times 0.0225 \times 5} \\ &= \frac{1150}{16.875} \\ &= 68.15 \text{ metres} \end{aligned}$$

Now check against table B1

Why are slabs bonded under wet areas?



No Earth? Ω ?



Bonded Slab

FLI < much lower