

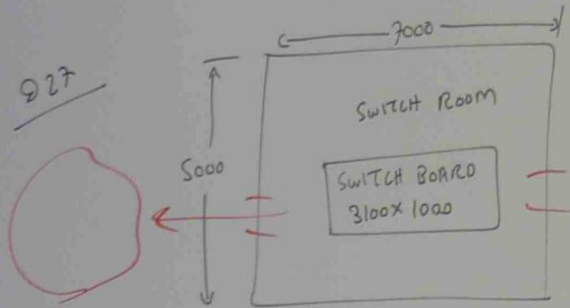
Q25 NAME TWO MATERIALS SUITABLE FOR THE CONSTRUCTION OF SWITCH BOARD SURMOUNTS.

METAL | CONCRETE

Q26 THE MAXIMUM NUMBER OF SWITCHES CLASSIFIED AS MAIN SWITCH IN ANY ONE INSTALLATION IS

6

Q27



THE GIVEN DIAGRAM REPRESENTS A SWITCH BOARD LOCATED IN A SWITCH ROOM. REFER AS 3000 AND ANSWER THE FOLLOWING QUESTIONS

- (a) HOW MANY EXITS ARE REQUIRED? SUFFICIENT
- (b) WHICH DIRECTION WILL THE EXIT DOOR SWING?
- (c) WHAT IDENTIFICATION MUST BE PLACED ON THE EXIT DOORS? SWITCH BOARD

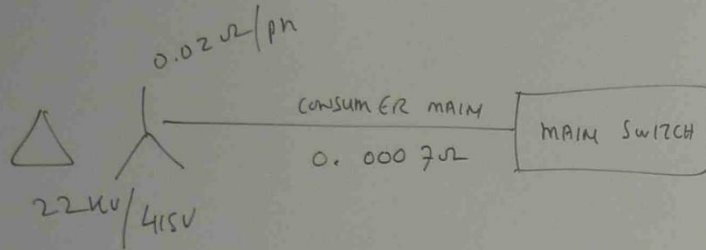
Q28 WHAT IS THE SIZE OF EXIT DOOR?  $0.75\text{m} \times 0.43\text{m}$

Q29 CALCULATE THE FAULT CURRENT AT A MAIN SWITCH BOARD THAT IS BEING SUPPLIED BY A 500 KVA  $\Delta$  22KV/415V TRANSFORMER WITH A PHASE IMPEDANCE  $0.02\Omega$  WHICH IS CONNECTED THROUGH A CONSUMER MAIN WITH IMPEDANCE  $0.0007\Omega$ .

Q 27(b)

DOOR OF SWITCH ROOM (OR) OTHER ROOMS DEDICATED TO SWITCH BOARD SHALL OPEN IN THE DIRECTION OF EGRESS WITHOUT THE USE ON THE SWITCH BOARD SIDE OF THE DOOR OF A KEY TOOL.

Q 29



$$I_{FL} = \frac{kVA \times 10^3}{\sqrt{3} E} = \frac{500 \times 10^3}{1.7321 \times 415} = 695 \text{ Amp.}$$

$$\begin{aligned} \% X &= \frac{I_{FL} \times X_{ph}}{E_{ph}} \times 100 \\ &= \frac{695 \times (0.0207)}{\left(\frac{415}{\sqrt{3}}\right)} \times 100 \\ &= 5.99 \% \end{aligned}$$

$$\begin{aligned} I_{Sh} &= \frac{I_{FL}}{\% X} \times 100 \\ &= \frac{695}{5.99} \times 100 \\ &= 11602 \text{ Amp.} \end{aligned}$$

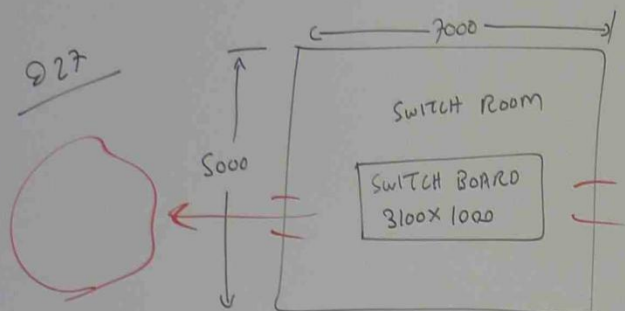
Q25. NAME TWO MATERIALS SUITABLE FOR THE CONSTRUCTION OF SWITCH BOARD SURROUNDS.

METAL | CONCRETE

Q26. THE MAXIMUM NUMBER OF SWITCHES CLASSED AS MAIN SWITCH IN ANY ONE INSTALLATION IS

6

Q27



THE GIVEN DIAGRAM REPRESENTS A SWITCH BOARD LOCATED IN A SWITCH ROOM. REFER AS 3000 AND ANSWER THE FOLLOWING QUESTIONS

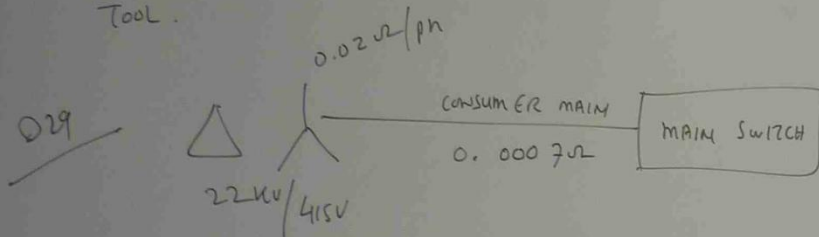
- (a) HOW MANY EXITS ARE REQUIRED? SUFFICIENT
- (b) WHICH DIRECTION WILL THE EXIT DOOR SWING?
- (c) WHAT IDENTIFICATION MUST BE PLACED ON THE EXIT DOORS? SWITCH BOARD

Q28. WHAT IS THE SIZE OF EXIT DOOR?  $0.75\text{m} \times 0.48\text{m}$

Q29. CALCULATE THE FAULT CURRENT AT A MAIN SWITCH BOARD THAT IS BEING SUPPLIED BY A 500 KVA  $\Delta$  22KV/415V TRANSFORMER WITH A PHASE IMPEDANCE  $0.02\Omega$  WHICH IS CONNECTED THROUGH A CONSUMER MAIN WITH IMPEDANCE  $0.0007\Omega$ .

Q 27 (b)

DOOR OF SWITCH ROOM (OR) OTHER ROOMS DEDICATED TO SWITCH BOARD SHALL OPEN IN THE DIRECTION OF EGRESS WITHOUT THE USE ON THE SWITCH BOARD SIDE OF THE DOOR OF A KEY TOOL.



$$I_{fL} = \frac{KVA \times 10^3}{\sqrt{3} E} = \frac{500 \times 10^3}{1.7321 \times 415} = 695 \text{ Amp.}$$

$$\% X = \frac{I_{fL} \times X_{ph}}{E_{ph}} \times 100$$

$$= \frac{695 \times (0.0207)}{\left(\frac{415}{\sqrt{3}}\right)} \times 100$$

$$= 5.99 \%$$

$$I_{Sh} = \frac{I_{fL}}{\% X} \times 100$$

$$= \frac{695}{5.99} \times 100$$

$$= 11602 \text{ Amp.}$$

Q 30

AREAS WHERE COMBUSTIBLE DUSTS CREATE THE HAZARD ARE CLASSIFIED AS CLASS II

Q 31

AREAS WHERE FLAMMABLE GASES ARE LIKELY TO OCCUR IN NORMAL OPERATION ARE CLASSIFIED AS CLASS I ZONE (1)



Q32 AREAS WHERE EXPLOSIVE GASES ARE CONSTANTLY PRESENT ARE CLASSIFIED AS \_\_\_\_\_ . **CLASS 1 ZONE (0)**

Q33 EQUIPMENT MUST BE INSTALLED IN A CLASS 1 ZONE 0 HAZARDOUS AREA IN ACCORDANCE WITH **AS 2381** . |

Q34 THE WIRING SYSTEM USED EXTENSIVELY FOR CONTROL FUNCTIONS IN CLASS 1 ZONE 0 IS CLASSIFIED AS **Ex ia**

Q35 CABLE GLAND FOR EQUIPMENTS IN CLASS II HAZARDOUS AREA SHOULD HAVE THE RATING **DIP**

Q36 IS EQUIPMENT WITH A LIQUID DIELECTRIC HAVING A FLASH POINT LESS THAN 250°C PERMITTED IN HAZARDOUS AREA? **NO.**

1)

Q37

3 WIRING METHODS THAT MAY BE USED IN CLASS 1

ZONE 1 AREA ARE

MIMS

TPS IN CONDUIT

TPS

Q38

WHAT IS THE PURPOSE OF FLAME PATH IN EQUIPMENT LABELLED Ex d

A LOW INTERNAL EXPLOSION PRESSURE WITHOUT  
IGNITING EXTERNAL GASES.

Q39

DESCRIPTION OF AREA

CLASS DESCRIPTION

WHEAT HANDLING

C II

FUME EXTRACTION IN A

C I

FURNITURE VARNISHING AREA

WOOD AND DUST EXTRACTION

C II

SYSTEM

UNDERGROUND PIT IN SERVICE  
STATION

C I

METHYLATED SPIRIT BOTTLING  
PLANT

C I

INSIDE PETROL STATION

C I

CARBON BLACK PROCESS  
AREA

C II

INSIDE SEWAGE TREATMENT  
PLANT

C I

INSIDE PETROL STORAGE  
TANK

C I

U.G CAR PARK

C I

40) THREE WIRING METHODS THAT MAY BE USED IN CLASS 1, ZONE 1 AREA ARE  
MIMS      TPS      TP1 IN CONDUIT

41) WHAT IS THE PURPOSE OF THE FLAME PATH IN EQUIPMENTS LABELLED Exd?

42) ARE WIRING SYSTEMS SUITABLE FOR CLASS 1 ZONE II ALWAYS SUITABLE FOR USE IN CLASS 1 ZONE 1 AREA?

43) NAME THREE TYPES OF EQUIPMENT THAT AS 3000 SPECIALLY EXCLUDES FROM USE IN HAZARDOUS LOCATIONS.

44) BRIEFLY DESCRIBE THE DIFFERENCE BETWEEN A MIMS STANDARD GLAND PATTERN AND A FLAME PROOF (OR) Exd PATTERN

45) ARE WIRING SYSTEMS FOR CLASS 1 AREAS ACCEPTABLE AS WIRING SYSTEMS IN CLASS II AREA?



46 NAME TWO WIRING SYSTEMS SPECIALLY EXCLUDED BY  
AS 3000 FOR USE IN CLASS II AREA.

47 WHICH TYPE OF LIGHT FITTING MAY BE INSTALLED IN (OR)  
ABOVE A CLASS I ZONE I AREA?

48 WHICH ELECTRICAL SYSTEM IS PERMITTED FOR USE IN ALL  
HAZARDOUS LOCATIONS?

49 DOES A CONDUIT (OR) PIPE CARRYING THE SUPPLY CABLE  
FROM THE OPERATOR'S CONSOLE TO THE PETROL PUMP IN  
SERVING STATION NEED TO BE SEALED WHERE IT ENTERS  
THE CONSOLE AREA?

(41) Exd

ALLOW INTERNAL EXPLOSION PRESSURE WITHOUT  
IGNITING EXTERNAL GASES

(42) NO

(43) BATTERY CHARGER  
SODIUM VAPOUR LAMP  
DIELECTRIC WITH FLASH POINT LESS THAN 250°C

(44) Exd LARGER THREAD LENGTH

(45) NOT ALWAYS

(46) BARE CONDUCTOR, OPEN WIRING

(47) TOTALLY ENCLOSED, FITTED WITH GLAND  
NO LOW PRESSURE SODIUM LAMP

(48) INTRINSIC SAFETY  
SPECIAL PRECAUTION

(49) NO.

- OVER CURRENT PROTECTION, OVER LOAD & SHORT CIRCUIT  
(RS 3000:2007 CLAUSE 2.5.3 & 2.5.4)
- PROTECTION AGAINST SWITCH BOARD ARCING FAULTS BY INTERNAL SEPARATION (OR) LIMITATION BY PROTECTIVE DEVICES  
(CLAUSE 2.5.5)
- RELIABILITY OF SUPPLY, CO-ORDINATION & DISCRIMINATION  
(CLAUSE 2.5.7)
- OVER CURRENT PROTECTION (1.5.9)
  - AUTOMATIC DISCONNECT
  - LIMITING MAXIMUM OVER CURRENT TO SAFE VALUE & DURATION

## 2.5.5 SWITCH BOARD INTERNAL ARCING FAULT PROTECTION

- SAFE OPERATION, INSPECTION, TESTING, MAINTENANCE
- DO NOT CAUSE DANGER FROM ELECTRIC SHOCK

SAFE WORKING DISTANCE FOR L.V = 500mm FROM  
LIVE PART

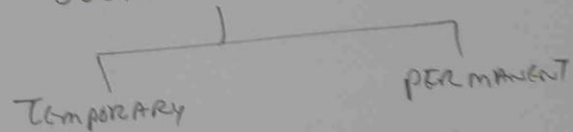
## 2.5.7 RELIABILITY OF SUPPLY

- 1.6.1 (b) FUNCTION CORRECTLY AS INTENDED  
(c) CONNECT, OPERATE SAFELY, BE COMPATIBLE WITH ELECTRICITY DISTRIBUTION SYSTEM  
(d) MINIMISE INCONVENIENCE IN CASE OF A FAULT

### PROTECTION AGAINST OVER CURRENT

- SUPPLY INFORMATION
- PROSPECTIVE (OR) DEEMED SHORT CIRCUIT CURRENT AT THE POINT OF SUPPLY
- 1.6.2 (f) PROSPECTIVE SHORT CIRCUIT CURRENT
  - SERVICE RULE
  - ARCLING FAULT LEVEL 60% AND 30%

### 1.4.38 OVER LOAD CURRENT



### 1.4.39 SHORT CIRCUIT CURRENT

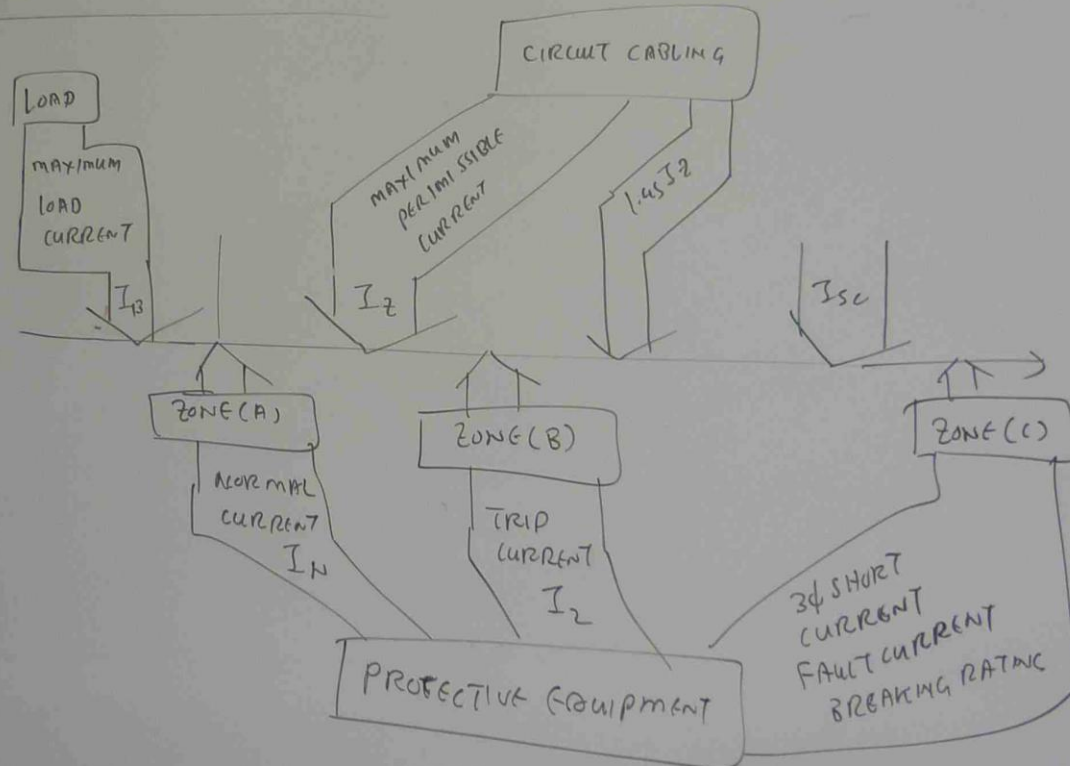
FAULT CURRENT RESULTING FROM A FAULT OF NEGLIGIBLE IMPEDANCE BETWEEN LIVE CONDUCTORS HAVING A DIFFERENCE OF POTENTIAL UNDER NORMAL OPERATION CONDITION.



NOT LESS THAN THE SIZE OF  
3.5.2 NEUTRAL CONDUCTOR SIZE = LARGEST ACTIVE CONDUCTOR

S. 3.3.1.2 EARTH CONDUCTOR = NOT LESS THAN 25% OF THE SIZE  
OF ACTIVE CONDUCTOR

### CABLE PROTECTION REQUIREMENT



ZONE (A)

ZONE (B)

ZONE (C)

ZONE (A)	$I_B \sqrt{I_N \sqrt{I_2}}$ ←	2.5.3.1	EQUATION 2.1 OVER LOAD
ZONE (B)	$I_2 \sqrt{1.45 I_2}$ ←	2.5.3.1	EQUATION 2.2 OVER LOAD
ZONE (C)	$I^2 t = K^2 S^2$ ←	2.5.4.5	EQUATION 2.4 SHORT CIRCUIT

$$S = C.SA \text{ mm}^2$$

$I$  = CURRENT

$t$  = TIME

$K$  = CONSTANT

