

$$(\alpha h)^4 = \left(\frac{\text{copper width}}{\text{slot width}} \times \text{solid cond. depth} \right)^4$$

∴ 0.097. The avg. loss factor is

$$K_{d\text{av}} = 1 + (\alpha h)^4 \left(\frac{m^2}{9} \right) \quad m = \text{no. of layers}$$

$$= 1 + 0.097 \left(\frac{5}{9} \right)$$

= 1.27 & the loss in the top layer

$$K_{d5} = 1 + 0.097 \left(\frac{20}{3} \right) = 1.66$$

Stray loss will be taken as 20%.

$$I^2R \text{ loss: } 3 \times 219^2 \times 0.000102 = 14.7 \text{ W}$$

$$\text{Eddy loss: } 0.27 \times 14.7 = 3.0 \text{ W}$$

$$\text{Stray loss: } 0.2 (14.7 + 3) = 3.5$$

$$\text{The IR drop is } 219 \times 102 \times 1.27 = 28.4 \text{ V}$$

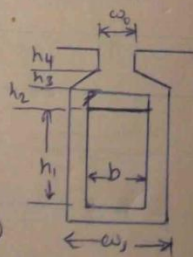
$$\text{The effective resistance is } \frac{28.4 \times 100}{3300/\sqrt{3}} = 1.5\% \text{ or } 0.05 \text{ pu}$$

Leakage reactance

The specific plot
permeance,

$$\lambda_s = \frac{h_1}{3\omega_1} + \frac{h_2}{\omega_2} + \frac{2h_3}{\omega_3 + \omega_4} + \frac{h_4}{\omega_5} \quad (60)$$

$$= \frac{41.7}{3 \times 13.5} + \frac{4}{13.5} + \frac{2 \times 2.8}{13.5 + 3} + \frac{1.5}{3} = 2.13$$



$$\begin{aligned} \text{slot leakage flux } \phi_s &= 2\sqrt{2} \mu_0 J T_c L_0 \lambda_s \quad (69) \\ &= 2\sqrt{2} (4\pi \times 10^{-7}) (5) (0.219) (2.13) \\ &= 2.45 \text{ mwb.} \end{aligned}$$

$$\begin{aligned} L_0 \lambda_0 &= K_s Y^2 / \pi g_s \quad (68) \\ &= 1 \times 0.298^2 / (\pi \times 0.0321) = 0.856 \end{aligned}$$

$$\begin{aligned} \phi_0 &= 2\sqrt{2} \mu_0 J T_c L_0 \lambda_0 \quad (70) \\ &= 2\sqrt{2} \times (4\pi \times 10^{-7}) \times 5 \times 219 \times 0.856 = 3.9 \text{ mwb.} \end{aligned}$$

The total leakage flux is $\phi_s + \phi_0 = 6.35 \text{ mwb.}$

Expressing this intensity of the main flux, $\frac{6.35}{57.6} = 0.11 \text{ p.u.}$

Stator core

For a core density of about 1.1 wb/m^2 , the depth h below the slot must accommodate half the flux; whence $h \approx 10 \text{ cm}$. The stator bore is $D = 130 \text{ cm}$, depth of two slot $b \approx 10.6 \text{ cm}$, so that the outside diameter of the stator core may be

$$D_o = 130 + 10.6 + 20 = 220 \text{ cm} = 2.2 \text{ m}$$

Air gap

The ratio of the field mmt on open ckt for normal vty. to the armature mmt at full load (ie the short ckt ratio) is 1.2. The armature mmt is

$$F_a = 1.35 J T_{ph} K_{a1} / p \quad (85)$$

$$= 1.35 \times 219 \times 150 \times 0.855 / 10 = 4240 \text{ AT/pole}$$