

LECTURE NOTES 18.75

The Relativistic Version of Maxwell's Stress Tensor $T^{\mu\nu}$

Despite the fact that we know that the *EM* energy density $u_{EM} = \frac{1}{2} \epsilon_o E^2 + \frac{1}{2\mu_o} B^2$ and Poynting's Vector, $\vec{S} = \frac{1}{\mu_o} \vec{E} \times \vec{B}$ are not Lorentz invariant quantities, we ask: Is there a related entity, relativistic in nature, from which we can understand the transformation properties of u_{EM} and \vec{S} , in going from one IRF(*S*) to another IRF(*S'*)?

The answer is yes – the 4-dimensional relativistic generalization of the 3-dimensional classical electrodynamics Maxwell's stress tensor: $\vec{T}_{ij} \rightarrow T^{\mu\nu}$!!!

Recall that the classical-electrodynamics 3-dimensional Maxwell stress tensor is \vec{T} , a 9-component, rank two 3×3 symmetric tensor (i.e. a matrix) whose elements are:

n.b. T_{ij} elements are symmetric:
 $T_{ij} = T_{ji} \Rightarrow \vec{T}$
 is a symmetric
 rank-2 tensor.

$\Rightarrow T_{ij} \equiv \epsilon_o \left(E_i E_j - \frac{1}{2} \delta_{ij} E^2 \right) + \frac{1}{\mu_o} \left(B_i B_j - \frac{1}{2} \delta_{ij} B^2 \right)$

where: $i, j = 1:3$

The Kronecker δ -function: $\delta_{ij} = \begin{cases} 1 & \text{if } i = j \\ 0 & \text{if } i \neq j \end{cases}$

Physically, \vec{T} is the force per unit area (or stress) acting on a surface of interest.

$T_{ij} \equiv$ force per unit area in i^{th} direction acting on an element of surface in the j^{th} direction.

\Rightarrow Thus: T_{xx}, T_{yy}, T_{zz} , physically represent pressures. (SI units: N/m^2)

\Rightarrow And: $T_{xy}, T_{xz}, T_{yx}, T_{yz}, T_{zx}, T_{zy}$ physically represent shears. (SI units: N/m^2)

n.b. SI units of \vec{T} all same (= pressure):

$$\frac{N}{m^2} = \frac{kg \cdot m / s^2}{m^2} = \frac{kg}{m \cdot s^2}$$

= Same SI units as energy density

$$\frac{J}{m^3} = \frac{N \cdot m}{m^3} = \frac{N}{m^2}$$

In classical electrodynamics, the force per unit volume (aka force density) is:

$$\vec{f}(\vec{r}, t) = \nabla \cdot \vec{T}(\vec{r}, t) - \frac{1}{c^2} \frac{\partial \vec{S}(\vec{r}, t)}{\partial t}$$

where:

$$\vec{S}(\vec{r}, t) = \frac{1}{\mu_o} \vec{E}(\vec{r}, t) \times \vec{B}(\vec{r}, t) = \text{Poynting's Vector}$$

SI units of force density: N/m^3
 = energy flux (watts/m²) through surface

The total force is therefore:

$$\vec{F}(t) = \int_v \vec{f}(\vec{r}, t) d\tau = \int_v \left(\nabla \cdot \vec{T}(\vec{r}, t) \right) d\tau - \frac{1}{c^2} \int_v \frac{\partial \vec{S}(\vec{r}, t)}{\partial t} d\tau$$

SI units of force =
 $N = kg \cdot m / s^2$

Use the divergence theorem on the 1st integral:

$$\vec{F}(t) = \oint_s \vec{T}(\vec{r}, t) \cdot d\vec{a} - \frac{1}{c^2} \int_v \frac{\partial \vec{S}(\vec{r}, t)}{\partial t} d\tau$$

In going from the classical electrodynamics 3-D spatial version of Maxwell's stress tensor \vec{T} a $3 \times 3 = 9$ element symmetric rank two tensor T_{ij}

$$T_{ij} \equiv \epsilon_0 \left(E_i E_j - \frac{1}{2} \delta_{ij} E^2 \right) + \frac{1}{\mu_0} \left(B_i B_j - \frac{1}{2} \delta_{ij} B^2 \right) = \epsilon_0 c^2 \left[\left(\frac{E_i}{c} \frac{E_j}{c} + B_i B_j \right) - \frac{1}{2} \delta_{ij} \left(\frac{E^2}{c^2} + B^2 \right) \right] \quad c^2 = \frac{1}{\epsilon_0 \mu_0}$$

$i, j = 1:3$

to the relativistic 4-dimensional space-time version of Maxwell's stress tensor $T^{\mu\nu}$ a $4 \times 4 = 16$ element symmetric tensor ($\mu, \nu = 0:3$) we expect the “new”/additional temporal components of $T^{\mu\nu}$ i.e. a new row (row # $\mu = 0$ column # $\nu = 0:3$) and a new LHS column (row # $\mu = 0:3$, column # $\nu = 0$) to:

- be symmetric, i.e. $T^{0\nu} = +T^{\nu 0}$
- have the same physical SI units ($N/m^2 = \text{pressure/energy density}$) as \vec{T}_{ij}
- have something to do with the temporal aspects of *EM* field energy flow
- be related to the *EM* field tensor, $F^{\mu\nu}$ (or equivalently, $G^{\mu\nu}$)

We define the relativistic version of Maxwell's stress tensor as:

$$T^{\mu\nu} \equiv \epsilon_0 c^2 \left[\left(F^{\mu\sigma} F^{\nu}_{\sigma} \right) - \frac{1}{4} \delta^{\mu\nu} \left(F_{\lambda\sigma} F^{\lambda\sigma} \right) \right] \quad \{\text{n.b. implicit sum over repeated indices!}\}$$

Where the “flat” space-time metric tensor, $\delta^{\mu\nu}$ (analogous to δ_{ij}) is defined as:

$$\delta^{\mu\nu} \equiv \begin{pmatrix} -1 & 0 & 0 & 0 \\ 0 & +1 & 0 & 0 \\ 0 & 0 & +1 & 0 \\ 0 & 0 & 0 & +1 \end{pmatrix} \quad \text{where:} \quad \delta^{\mu\nu} \equiv \begin{cases} -1 & \text{for } \mu = \nu = 0 \\ +1 & \text{for } \mu = \nu = 1, 2, 3 \\ 0 & \text{for } \mu \neq \nu \end{cases}$$

Note that the differences in the physical appearance between definitions of 3-D \vec{T}_{ij} and 4-D $T^{\mu\nu}$

$$T_{ij} \equiv \epsilon_0 c^2 \left[\left(\frac{E_i}{c} \frac{E_j}{c} + B_i B_j \right) - \frac{1}{2} \delta_{ij} \left(\frac{E^2}{c^2} + B^2 \right) \right] \quad \delta_{ij} \equiv \begin{pmatrix} +1 & & & \\ & +1 & & \\ & & +1 & \\ & & & +1 \end{pmatrix}$$

$$T^{\mu\nu} \equiv \epsilon_0 c^2 \left[\left(F^{\mu\sigma} F^{\nu}_{\sigma} \right) - \frac{1}{4} \delta^{\mu\nu} \left(F_{\lambda\sigma} F^{\lambda\sigma} \right) \right] \quad \delta^{\mu\nu} \equiv \begin{pmatrix} -1 & & & \\ & +1 & & \\ & & +1 & \\ & & & +1 \end{pmatrix}$$

n.b. symmetric tensors, SI units:
 $N/m^2 = \frac{kg}{m-s^2}$

arise from our (& Griffiths') definition of the anti-symmetric *EM* field tensor, $F^{\mu\nu}$:

$$F^{\mu\nu} \equiv \begin{pmatrix} 0 & \frac{E_x}{c} & \frac{E_y}{c} & \frac{E_z}{c} \\ -\frac{E_x}{c} & 0 & B_z & -B_y \\ -\frac{E_y}{c} & B_z & 0 & B_x \\ -\frac{E_z}{c} & B_y & -B_x & 0 \end{pmatrix} \quad \text{and:} \quad \boxed{(F_{\lambda\sigma} F^{\lambda\sigma}) = 2 \left(B^2 - \frac{1}{c^2} E^2 \right) = -2 \left(\frac{E^2}{c^2} - B^2 \right)}$$

(See Griffiths problem 12.50, p. 537 P436 HW #14)

For clarity's sake, here we present the results for $T^{\mu\nu}$ and place the (tedious!) calculational details in Appendix "A" of these lecture notes.

Recall that Poynting's Vector, $\vec{S} = \frac{1}{\mu_o} (\vec{E} \times \vec{B})$ SI units: $\text{Watts}/m^2 = \frac{J/s}{m^2} = \frac{J}{m^2 \cdot s} = \frac{N \cdot m}{m^2 \cdot s} = \frac{N}{m \cdot s}$

Recall that EM field linear momentum density: $\vec{\phi}_{EM} \equiv \epsilon_o (\vec{E} \times \vec{B})$

$$\vec{\phi}_{EM} \equiv \epsilon_o (\vec{E} \times \vec{B}) = \epsilon_o \mu_o \left[\frac{1}{\mu_o} (\vec{E} \times \vec{B}) \right] = \epsilon_o \mu_o \vec{S} = \frac{1}{c^2} \vec{S} \quad \leftarrow \quad \frac{1}{c^2} = \epsilon_o \mu_o$$

$$\therefore \vec{\phi}_{EM} c = \frac{1}{c} \vec{S} = \frac{1}{c} \left[\frac{1}{\mu_o} (\vec{E} \times \vec{B}) \right] = \frac{1}{\mu_o} \left[\left(\frac{\vec{E}}{c} \times \vec{B} \right) \right] = \epsilon_o c^2 \left(\frac{\vec{E}}{c} \times \vec{B} \right)$$

SI units of $\vec{\phi}_{EM} c = \frac{1}{c} \vec{S}$: $\frac{kg}{m^2 \cdot s} \cdot \frac{m}{s} = \frac{kg}{m \cdot s^2}$ but: $1N = kg \cdot m/s^2$

$$= \frac{kg \cdot m}{m^2 \cdot s^2} = \frac{N}{m^2} = \text{pressure} = \frac{N \cdot m}{m^3} = \frac{J}{m^3} = \text{energy density}$$

Recall that the EM field energy density u_{EM} is defined as:

$$u_{EM} \equiv \frac{1}{2} \epsilon_o E^2 + \frac{1}{2 \mu_o} B^2 = \frac{1}{2} \epsilon_o (\vec{E} \cdot \vec{E}) + \frac{1}{2 \mu_o} \vec{B} \cdot \vec{B} = \frac{1}{2} \epsilon_o c^2 \left(\frac{E^2}{c^2} \right) + \frac{1}{2} \epsilon_o c^2 B^2 = \frac{1}{2} \epsilon_o c^2 \left[\left(\frac{E^2}{c^2} \right) + B^2 \right]$$

SI units: $\frac{J}{m^3} = \frac{N \cdot m}{m^3} = \frac{N}{m^2} = \text{energy density} = \text{pressure} = \text{force per unit area}$

= {linear} momentum flux density

Explicitly reminding the reader that the 3-D classical electrodynamics version of Maxwell's stress tensor \vec{T} is defined as:

Column # $j = 1:3$
 $1=x \quad 2=y \quad 3=z$ Row # $i = 1:3$
 $1=x \quad 2=y \quad 3=z$

$$\vec{T} = T_{ij} = \begin{pmatrix} T_{xx} & T_{xy} & T_{xz} \\ T_{yx} & T_{yy} & T_{yz} \\ T_{zx} & T_{zy} & T_{zz} \end{pmatrix} = \epsilon_o c^2 \left[\left(\frac{E_i E_j}{c} + B_i B_j \right) - \frac{1}{2} \delta_{ij} \left(\frac{E^2}{c^2} + B^2 \right) \right] \quad \delta_{ij} = \begin{cases} 1 & \text{if } i = j \\ 0 & \text{if } i \neq j \end{cases}$$

Row # Column #
 (1:3) (1:3)

$$\vec{T} = \begin{pmatrix} \epsilon_o c^2 \left[\left(\frac{E_x^2}{c^2} + B_x^2 \right) - \frac{1}{2} \left(\frac{E^2}{c^2} + B^2 \right) \right] & \epsilon_o c^2 \left[\frac{E_x E_y}{c} + B_x B_y \right] & \epsilon_o c^2 \left[\frac{E_x E_z}{c} + B_x B_z \right] \\ \epsilon_o c^2 \left[\frac{E_y E_x}{c} + B_y B_x \right] & \epsilon_o c^2 \left[\left(\frac{E_y^2}{c^2} + B_y^2 \right) - \frac{1}{2} \left(\frac{E^2}{c^2} + B^2 \right) \right] & \epsilon_o c^2 \left[\frac{E_y E_z}{c} + B_y B_z \right] \\ \epsilon_o c^2 \left[\frac{E_z E_x}{c} + B_z B_x \right] & \epsilon_o c^2 \left[\frac{E_z E_y}{c} + B_z B_y \right] & \epsilon_o c^2 \left[\left(\frac{E_z^2}{c^2} + B_z^2 \right) - \frac{1}{2} \left(\frac{E^2}{c^2} + B^2 \right) \right] \end{pmatrix}$$

$$\vec{T} = \frac{1}{2} \epsilon_o c^2 \begin{pmatrix} \left(\frac{E_x^2}{c^2} - \frac{E_y^2}{c^2} - \frac{E_z^2}{c^2} \right) + (B_x^2 - B_y^2 - B_z^2) & 2 \left[\frac{E_x E_y}{c} + B_x B_y \right] & 2 \left[\frac{E_x E_z}{c} + B_x B_z \right] \\ 2 \left[\frac{E_y E_x}{c} + B_y B_x \right] & \left(\frac{E_y^2}{c^2} + B_y^2 \right) + (-B_x^2 + B_y^2 - B_z^2) & 2 \left[\frac{E_y E_z}{c} + B_y B_z \right] \\ 2 \left[\frac{E_z E_x}{c} + B_z B_x \right] & 2 \left[\frac{E_z E_y}{c} + B_z B_y \right] & \left(-\frac{E_x^2}{c^2} - \frac{E_y^2}{c^2} + \frac{E_z^2}{c^2} \right) + (-B_x^2 - B_y^2 + B_z^2) \end{pmatrix}$$

\Rightarrow Note that the T_{ij} elements are symmetric, i.e. $T_{ji} = T_{ij}$

Physically:

T_{ij} ($i, j = 1:3$) are pure space-space components.

$T_{ij} = i^{th}$ component of force across unit area perpendicular to j^{th} direction.

$T_{ii} = T_{xx}, T_{yy}, T_{zz}$ represent pressures on enclosing surfaces in the x, y, z directions, respectively.

$T_{ij} = (T_{xy} = T_{yx}), (T_{xz} = T_{zx}), (T_{yz} = T_{zy})$ represent stresses (or shears) on enclosing surfaces in the x, y , or z directions

But note also that physically:

$T_{ij} = -ve$ of the rate of flow of the i^{th} component of EM field linear momentum \vec{p} through unit area whose normal is in the j^{th} direction, i.e. $-T_{ij}$ is the i^{th} component of the linear momentum flux density transported in the j^{th} direction by the EM fields.

Then, the relativistic 4-D space-time version of Maxwell's stress tensor defined as:

$$T^{\mu\nu} \equiv \epsilon_o c^2 \left[\left(F^{\mu\sigma} F^\nu{}_\sigma \right) - \frac{1}{4} \delta^{\mu\nu} \left(F_{\lambda\sigma} F^{\lambda\sigma} \right) \right] \quad \text{gives:}$$

Row #	Column #	Column #	Row #
		0=t 1=x 2=y 3=z	
0:3	0:3	$T^{\mu\nu} = \begin{pmatrix} T^{00} & T^{01} & T^{02} & T^{03} \\ T^{10} & T^{11} & T^{12} & T^{13} \\ T^{20} & T^{21} & T^{22} & T^{23} \\ T^{30} & T^{31} & T^{32} & T^{33} \end{pmatrix}$	0=t 1=x 2=y 3=z
		$= \begin{pmatrix} T^{tt} & T^{tx} & T^{ty} & T^{tz} \\ T^{xt} & T^{xx} & T^{xy} & T^{xz} \\ T^{yt} & T^{yx} & T^{yy} & T^{yz} \\ T^{zt} & T^{zx} & T^{zy} & T^{zz} \end{pmatrix}$	

Now while we might hope that the $\{\mu, \nu = 1:3\}$ pure space-space elements of the relativistic 4-D space-time stress tensor $T^{\mu\nu}$ would be identical to that of the 3-D classical electrodynamics / Maxwell's stress tensor \vec{T}_{ij} , because of our definitions for $T^{\mu\nu}$ and $F^{\mu\nu}$ what we instead obtain is:

$$T^{\mu\nu} \Big|_{\mu, \nu=1:3} = -\vec{T}_{ij} \Big|_{i, j=1:3}$$

Thus, we see that the pure space-space $\{\mu, \nu = 1:3\}$ components of the relativistic stress tensor $T^{\mu\nu}$ physically represent EM field linear momentum flux densities, the negative of which physically corresponds to stresses/shears on bounding surfaces!

The temporal components of $T^{\mu\nu}$ are:

$\nu = 0$ (1st column):

$$\frac{1}{\mu_o} = \epsilon_o c^2$$

$$\begin{aligned} T^{00} &= u_{EM} = \frac{1}{2} \epsilon_o E^2 + \frac{1}{2\mu_o} B^2 = \frac{1}{2} \epsilon_o c^2 \left(\frac{E^2}{c^2} + B^2 \right) \\ T^{10} &= \wp_x c = \epsilon_o c^2 \left(\frac{E_y}{c} B_z - \frac{E_z}{c} B_y \right) = \epsilon_o c (E_y B_z - E_z B_y) \\ T^{20} &= \wp_y c = \epsilon_o c^2 \left(\frac{E_z}{c} B_x - \frac{E_x}{c} B_z \right) = \epsilon_o c (E_z B_x - E_x B_z) \\ T^{30} &= \wp_z c = \epsilon_o c^2 \left(\frac{E_x}{c} B_y - \frac{E_y}{c} B_x \right) = \epsilon_o c (E_x B_y - E_y B_x) \end{aligned}$$

Recalling that Poynting's Vector: $\vec{S} \equiv \frac{1}{\mu_o} (\vec{E} \times \vec{B}) \quad \therefore \quad \frac{1}{c} \vec{S} = \frac{1}{\mu_o} \left(\frac{\vec{E}}{c} \times \vec{B} \right) = \epsilon_o c^2 \left(\frac{\vec{E}}{c} \times \vec{B} \right) = \epsilon_o c (\vec{E} \times \vec{B})$

Thus: $\frac{1}{c} \vec{S} = \frac{1}{c} S_x \hat{x} + \frac{1}{c} S_y \hat{y} + \frac{1}{c} S_z \hat{z} = \epsilon_o c (E_y B_z - E_z B_y) \hat{x} + \epsilon_o c (E_z B_x - E_x B_z) \hat{y} + \epsilon_o c (E_x B_y - E_y B_x) \hat{z}$

$\mu = 0$ (1st row):

$$\begin{aligned} T^{01} &= \frac{1}{c} S_x = \epsilon_o c (E_y B_z - E_z B_y) \\ T^{02} &= \frac{1}{c} S_y = \epsilon_o c (E_z B_x - E_x B_z) \\ T^{03} &= \frac{1}{c} S_z = \epsilon_o c (E_x B_y - E_y B_x) \end{aligned}$$

Thus, we (explicitly) see that:

$$\begin{aligned} T^{10} = T^{01} &\Rightarrow \wp_x c = \frac{1}{c} S_x \\ T^{20} = T^{02} &\Rightarrow \wp_y c = \frac{1}{c} S_y \\ T^{30} = T^{03} &\Rightarrow \wp_z c = \frac{1}{c} S_z \end{aligned} \quad \left. \vphantom{\begin{aligned} T^{10} = T^{01} \\ T^{20} = T^{02} \\ T^{30} = T^{03} \end{aligned}} \right\} \text{ or: } \vec{\wp} c = \frac{1}{c} \vec{S} = \epsilon_o c (\vec{E} \times \vec{B})$$

Thus the components of the relativistic 4-D/spacetime version of Maxwell's stress tensor $T^{\mu\nu}$ are $\{T^{\mu\nu} = T^{\nu\mu} = \text{symmetric tensor}\}$: $T^{\mu\nu} \equiv \epsilon_o c^2 \left[(F^{\mu\sigma} F_{\sigma}^{\nu}) - \frac{1}{4} \delta^{\mu\nu} (F_{\lambda\sigma} F^{\lambda\sigma}) \right]$

$$T^{\mu\nu} = \begin{pmatrix} T^{00} & T^{01} & T^{02} & T^{03} \\ T^{10} & T^{11} & T^{12} & T^{13} \\ T^{20} & T^{21} & T^{22} & T^{23} \\ T^{30} & T^{31} & T^{32} & T^{33} \end{pmatrix} = \begin{pmatrix} T^{tt} & T^{tx} & T^{ty} & T^{tz} \\ T^{xt} & T^{xx} & T^{xy} & T^{xz} \\ T^{yt} & T^{yx} & T^{yy} & T^{yz} \\ T^{zt} & T^{zx} & T^{zy} & T^{zz} \end{pmatrix} = \begin{pmatrix} T^{tt} & T^{tx} & T^{ty} & T^{tz} \\ T^{xt} & -T_{xx} & -T_{xy} & -T_{xz} \\ T^{yt} & -T_{yx} & -T_{yy} & -T_{yz} \\ T^{zt} & -T_{zx} & -T_{zy} & -T_{zz} \end{pmatrix} \quad \left. \vphantom{\begin{pmatrix} T^{tt} & T^{tx} & T^{ty} & T^{tz} \\ T^{xt} & -T_{xx} & -T_{xy} & -T_{xz} \\ T^{yt} & -T_{yx} & -T_{yy} & -T_{yz} \\ T^{zt} & -T_{zx} & -T_{zy} & -T_{zz} \end{pmatrix}} \right\} \begin{array}{l} \text{3-D space-space components} \\ \text{of classical electrodynamics'} \\ \text{Maxwell's stress tensor } \vec{\vec{T}}_{ij} \end{array}$$

$$T^{\mu\nu} = \begin{pmatrix} u_{EM} = \frac{1}{2} \epsilon_o c^2 \left(\left(\frac{E}{c} \right)^2 + B^2 \right) & \frac{1}{c} S_x & \frac{1}{c} S_y & \frac{1}{c} S_z \\ \wp_x c & -\epsilon_o c^2 \left[\left(\frac{E_x^2}{c^2} + B_x^2 \right) - \frac{1}{2} \left(\frac{E^2}{c^2} + B^2 \right) \right] & -\epsilon_o c^2 \left[\left(\frac{E_x E_y}{c} \right) + (B_x B_y) \right] & -\epsilon_o c^2 \left[\left(\frac{E_x E_z}{c} \right) + (B_x B_z) \right] \\ \wp_y c & -\epsilon_o c^2 \left[\left(\frac{E_y E_x}{c} \right) + (B_y B_x) \right] & -\epsilon_o c^2 \left[\left(\frac{E_y^2}{c^2} + B_y^2 \right) - \frac{1}{2} \left(\frac{E^2}{c^2} + B^2 \right) \right] & -\epsilon_o c^2 \left[\left(\frac{E_y E_z}{c} \right) + (B_y B_z) \right] \\ \wp_z c & -\epsilon_o c^2 \left[\left(\frac{E_z E_x}{c} \right) + (B_z B_x) \right] & -\epsilon_o c^2 \left[\left(\frac{E_z E_y}{c} \right) + (B_z B_y) \right] & -\epsilon_o c^2 \left[\left(\frac{E_z^2}{c^2} + B_z^2 \right) - \frac{1}{2} \left(\frac{E^2}{c^2} + B^2 \right) \right] \end{pmatrix}$$

Physically:

$T^{\mu\nu} =$	EM field energy density, u_{EM}	x -flow of EM field energy, S_x/c	y -flow of EM field energy, S_y/c	z -flow of EM field energy, S_z/c
	flux of EM field momentum density, \wp_x	x – flow of EM field linear momentum density, \wp_x	y – flow of EM field linear momentum density, \wp_x	z – flow of EM field linear momentum density, \wp_x
	flux of EM field momentum density, \wp_y	x – flow of EM field linear momentum density, \wp_y	y – flow of EM field linear momentum density, \wp_y	z – flow of EM field linear momentum density, \wp_y
	flux of EM field momentum density, \wp_z	x – flow of EM field linear momentum density, \wp_z	y – flow of EM field linear momentum density, \wp_z	z – flow of EM field linear momentum density, \wp_z

SI units of $T^{\mu\nu}$: energy density = $J/m^2 = N\cdot m/m^2 = N/m^2 =$ pressure

$$T^{00} = u_{EM} = \frac{1}{2} \epsilon_o c^2 \left(\frac{E^2}{c^2} + B^2 \right) = \frac{1}{2} \epsilon_o E^2 + \frac{1}{2\mu_o} B^2 \quad \text{using:} \quad \left(c^2 = \frac{1}{\epsilon_o \mu_o} \right)$$

$$T^{10} = \wp_x c = \epsilon_o c^2 \left(\frac{E_y}{c} B_z - \frac{E_z}{c} B_y \right) = \epsilon_o c (E_y B_z - E_z B_y) = \frac{1}{c} S_x = T^{01}$$

$$T^{20} = \wp_y c = \epsilon_o c^2 \left(\frac{E_z}{c} B_x - \frac{E_x}{c} B_z \right) = \epsilon_o c (E_z B_x - E_x B_z) = \frac{1}{c} S_y = T^{02}$$

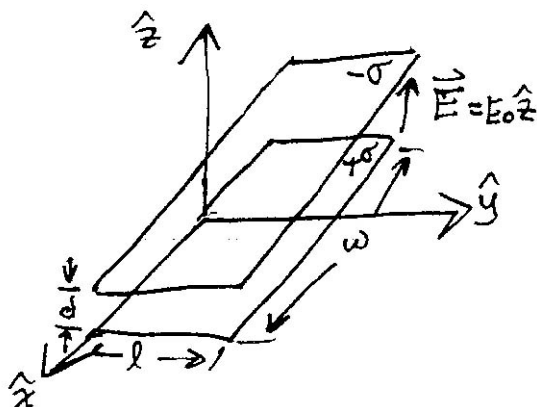
$$T^{30} = \wp_z c = \epsilon_o c^2 \left(\frac{E_x}{c} B_y - \frac{E_y}{c} B_x \right) = \epsilon_o c (E_x B_y - E_y B_x) = \frac{1}{c} S_z = T^{03}$$

$$T^{01} = \frac{1}{c} S_x = \epsilon_o c (\vec{E} \times \vec{B})_x = \epsilon_o c (E_y B_z - E_z B_y) = \wp_x c = T^{10}$$

$$T^{02} = \frac{1}{c} S_y = \epsilon_o c (\vec{E} \times \vec{B})_y = \epsilon_o c (E_z B_x - E_x B_z) = \wp_y c = T^{20}$$

$$T^{03} = \frac{1}{c} S_z = \epsilon_o c (\vec{E} \times \vec{B})_z = \epsilon_o c (E_x B_y - E_y B_x) = \wp_z c = T^{30}$$

As a simple example of the use of the 4-D/relativistic version of Maxwell's stress tensor $T^{\mu\nu}$, let us consider the purely electrostatic problem of a parallel-plate capacitor at rest in the lab frame IRF(S), with large area plates \parallel to the x - y plane as shown in the figure below:



Inside the \parallel plates $\{d \ll w, \ell\}$:

$$\vec{E} = E_o \hat{z} \quad (\vec{E} = 0 \text{ elsewhere})$$

$$\vec{B} = 0 \text{ everywhere}$$

Then:

$$T^{\mu\nu} = \begin{pmatrix} u_{EM} & \frac{1}{c} S_x & \frac{1}{c} S_y & \frac{1}{c} S_z \\ \rho_x c & -T_{xx} & -T_{xy} & -T_{xz} \\ \rho_y c & -T_{yx} & -T_{yy} & -T_{yz} \\ \rho_z c & -T_{zx} & -T_{zy} & -T_{zz} \end{pmatrix} = \begin{pmatrix} \frac{1}{2} \epsilon_o E_o^2 & 0 & 0 & 0 \\ 0 & +\frac{1}{2} \epsilon_o E_o^2 & 0 & 0 \\ 0 & 0 & +\frac{1}{2} \epsilon_o E_o^2 & 0 \\ 0 & 0 & 0 & -\frac{1}{2} \epsilon_o E_o^2 \end{pmatrix}$$

$$T^{\mu\nu} = \frac{1}{2} \epsilon_o E_o^2 \begin{pmatrix} +1 & 0 & 0 & 0 \\ 0 & +1 & 0 & 0 \\ 0 & 0 & +1 & 0 \\ 0 & 0 & 0 & -1 \end{pmatrix}$$

Only the diagonal elements
of $T^{\mu\nu} = T^{\mu\mu}$ are non-zero

$$T^{00} = u_{EM} = +\frac{1}{2} \epsilon_o E_o^2 \Rightarrow +ve \text{ Energy Density (J/m}^3\text{)}$$

$$T^{11} = -T_{xx} = +\frac{1}{2} \epsilon_o E_o^2 \Rightarrow +ve \text{ EM Pressure} = \left[+\frac{1}{2} \epsilon_o E_o^2 \right] \text{ in } \hat{x}\text{-direction !!!}$$

$$T^{22} = -T_{yy} = +\frac{1}{2} \epsilon_o E_o^2 \Rightarrow +ve \text{ EM Pressure} = \left[+\frac{1}{2} \epsilon_o E_o^2 \right] \text{ in } \hat{y}\text{-direction !!!}$$

$$T^{33} = -T_{zz} = -\frac{1}{2} \epsilon_o E_o^2 \Rightarrow -ve \text{ EM Pressure} = \left[-\frac{1}{2} \epsilon_o E_o^2 \right] \text{ in } \hat{z}\text{-direction \{n.b. } \vec{E} = E_o \hat{z} \} !!!}$$

\Rightarrow Plates of capacitor attracted to each other – net attractive force acting on bottom/top plates:

$$\text{Tension: } \vec{F}_{bot} = +\sigma \ell w E_o \hat{z} = +Q E_o \hat{z}, \quad \vec{F}_{top} = -\sigma \ell w E_o \hat{z} = -Q E_o \hat{z} = -\vec{F}_{bot}$$

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$$\begin{array}{c}
 \boxed{
 \begin{array}{cccc}
 F_{\lambda\sigma} F^{\lambda\sigma} = +0^2 & -(E_x/c)^2 & -(E_y/c)^2 & -(E_z/c)^2 \\
 -(-E_x/c)^2 & +0^2 & + (B_z)^2 & + (-B_y)^2 \\
 -(-E_y/c)^2 & + (B_z)^2 & +0^2 & + (B_x)^2 \\
 -(-E_z/c)^2 & + (B_y)^2 & + (-B_x)^2 & +0^2
 \end{array}
 } \Rightarrow \boxed{
 \begin{array}{l}
 F_{\lambda\sigma} F^{\lambda\sigma} = -\frac{E_x^2}{c^2} - \frac{E_y^2}{c^2} - \frac{E_z^2}{c^2} \\
 -\frac{E_x^2}{c^2} + B_z^2 + B_y^2 \\
 -\frac{E_y^2}{c^2} + B_z^2 + B_x^2 \\
 -\frac{E_z^2}{c^2} + B_y^2 + B_x^2
 \end{array}
 }
 \end{array}$$

$$F_{\lambda\sigma} F^{\lambda\sigma} = 2 \left[-\left(\frac{E_x^2}{c^2} + \frac{E_y^2}{c^2} + \frac{E_z^2}{c^2} \right) + (B_x^2 + B_y^2 + B_z^2) \right] = 2 \left(-\frac{E^2}{c^2} + B^2 \right) = 2 \left(B^2 - \frac{E^2}{c^2} \right) = -2 \left(\frac{E^2}{c^2} - B^2 \right)$$

$$\therefore \left(F_{\lambda\sigma} F^{\lambda\sigma} \right) = \left(F^{\lambda\sigma} F_{\lambda\sigma} \right) = 2 \left(B^2 - \frac{E^2}{c^2} \right) = -2 \left(\frac{E^2}{c^2} - B^2 \right)$$

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Next, we need to calculate $(F^{\mu\sigma} F^{\nu}_{\sigma})$ which is a $4 \times 4 = 16$ element tensor $= S^{\mu\nu}$

n.b. repeated indices (σ) are summed over $\sigma = 0:3$ for each element of $S^{\mu\nu}$!!!

Calculate the 16 elements of 4×4 tensor: $S^{\mu\nu} \equiv F^{\mu\sigma} F^{\nu}_{\sigma}$

$\nu = 0$ (1st column) of $S^{\mu\sigma}$ ($\mu = 0:3$):

$$S^{00} \equiv F^{0\sigma} F^0_{\sigma} = -F^{00} F^{00} + F^{01} F^{01} + F^{02} F^{02} + F^{03} F^{03} = -0^2 + \left(\frac{E_x}{c} \right)^2 + \left(\frac{E_y}{c} \right)^2 + \left(\frac{E_z}{c} \right)^2 = \frac{E^2}{c^2}$$

$$\begin{aligned}
 S^{10} &\equiv F^{1\sigma} F^0_{\sigma} = -F^{10} F^{00} + F^{11} F^{01} + F^{12} F^{02} + F^{13} F^{03} \\
 &= -\left(-\frac{E_x}{c} \right)(0) + (0) \left(\frac{E_x}{c} \right) + B_z \left(\frac{E_y}{c} \right) + (-B_y) \left(\frac{E_z}{c} \right) = \frac{1}{c} (E_y B_z - E_z B_y)
 \end{aligned}$$

$$\begin{aligned}
 S^{20} &\equiv F^{2\sigma} F^0_{\sigma} = -F^{20} F^{00} + F^{21} F^{01} + F^{22} F^{02} + F^{23} F^{03} \\
 &= -\left(-\frac{E_y}{c} \right)(0) + (-B_z) \left(\frac{E_x}{c} \right) + (0) \left(\frac{E_y}{c} \right) + (B_x) \left(\frac{E_z}{c} \right) = \frac{1}{c} (E_z B_x - E_x B_z)
 \end{aligned}$$

$$\begin{aligned}
 S^{30} &\equiv F^{3\sigma} F^0_{\sigma} = -F^{30} F^{00} + F^{31} F^{01} + F^{32} F^{02} + F^{33} F^{03} \\
 &= -\left(-\frac{E_z}{c} \right)(0) + (B_y) \left(\frac{E_x}{c} \right) + (-B_x) \left(\frac{E_y}{c} \right) + (0) \left(\frac{E_z}{c} \right) = \frac{1}{c} (E_x B_y - E_y B_x)
 \end{aligned}$$

$\nu = 1$ (2nd column) of $S^{\mu\sigma}$ ($\mu = 0:3$):

$$\begin{aligned} S^{01} &\equiv F^{0\sigma} F^1_{\sigma} = -F^{00} F^{10} + F^{01} F^{11} + F^{02} F^{12} + F^{03} F^{13} \\ &= -(0) \left(-\frac{E_x}{c} \right) + \left(\frac{E_x}{c} \right) (0) + \left(\frac{E_y}{c} \right) (B_z) + \left(\frac{E_z}{c} \right) (-B_y) = \frac{1}{c} (E_y B_z - E_z B_y) \end{aligned}$$

$$\begin{aligned} S^{11} &\equiv F^{1\sigma} F^1_{\sigma} = -F^{10} F^{10} + F^{11} F^{11} + F^{12} F^{12} + F^{13} F^{13} \\ &= -\left(-\frac{E_x}{c} \right) \left(-\frac{E_x}{c} \right) + (0)(0) + (B_z)(B_z) + (-B_y)(-B_y) = -\frac{E_x^2}{c^2} + B_y^2 + B_z^2 \end{aligned}$$

$$\begin{aligned} S^{21} &\equiv F^{2\sigma} F^1_{\sigma} = -F^{20} F^{10} + F^{21} F^{11} + F^{22} F^{12} + F^{23} F^{13} \\ &= -\left(-\frac{E_y}{c} \right) \left(-\frac{E_x}{c} \right) + (-B_z)(0) + (0)(B_z) + (B_x)(-B_y) = -\left(\frac{E_x E_y}{c^2} + B_x B_y \right) \end{aligned}$$

$$\begin{aligned} S^{31} &\equiv F^{3\sigma} F^1_{\sigma} = -F^{30} F^{10} + F^{31} F^{11} + F^{32} F^{12} + F^{33} F^{13} \\ &= -\left(-\frac{E_z}{c} \right) \left(-\frac{E_x}{c} \right) + (B_y)(0) + (-B_x)(B_z) + (0)(-B_y) = -\left(\frac{E_x E_z}{c^2} + B_x B_z \right) \end{aligned}$$

$\nu = 2$ (3rd column) of $S^{\mu\sigma}$ ($\mu = 0:3$):

$$\begin{aligned} S^{02} &\equiv F^{0\sigma} F^2_{\sigma} = -F^{00} F^{20} + F^{01} F^{21} + F^{02} F^{22} + F^{03} F^{23} \\ &= -(0) \left(-\frac{E_y}{c} \right) + \left(\frac{E_x}{c} \right) (-B_z) + \left(\frac{E_y}{c} \right) (0) + \left(\frac{E_z}{c} \right) (B_x) = \frac{1}{c} (E_z B_x - E_x B_z) \end{aligned}$$

$$\begin{aligned} S^{12} &\equiv F^{1\sigma} F^2_{\sigma} = -F^{10} F^{20} + F^{11} F^{21} + F^{12} F^{22} + F^{13} F^{23} \\ &= -\left(-\frac{E_x}{c} \right) \left(-\frac{E_y}{c} \right) + (0)(-B_z) + (B_z)(0) + (-B_y)(B_x) = -\left(\frac{E_x E_y}{c^2} + B_x B_y \right) \end{aligned}$$

$$\begin{aligned} S^{22} &\equiv F^{2\sigma} F^2_{\sigma} = -F^{20} F^{20} + F^{21} F^{21} + F^{22} F^{22} + F^{23} F^{23} \\ &= -\left(-\frac{E_y}{c} \right) \left(-\frac{E_y}{c} \right) + (-B_z)(-B_z) + (0)(0) + (B_x)(B_x) = -\frac{E_y^2}{c^2} + B_x^2 + B_z^2 \end{aligned}$$

$$\begin{aligned} S^{23} &\equiv F^{2\sigma} F^3_{\sigma} = -F^{20} F^{30} + F^{21} F^{31} + F^{22} F^{32} + F^{23} F^{33} \\ &= -\left(-\frac{E_y}{c} \right) \left(-\frac{E_z}{c} \right) + (B_y)(-B_z) + (-B_x)(0) + (0)(B_x) = -\left(\frac{E_y E_z}{c^2} + B_y B_z \right) \end{aligned}$$

$\nu = 3$ (4th column) of $S^{\mu\sigma}$ ($\mu = 0:3$):

$$\begin{aligned} S^{03} &\equiv F^{0\sigma} F^3_{\sigma} = -F^{00} F^{30} + F^{01} F^{31} + F^{02} F^{32} + F^{03} F^{33} \\ &= -(0) \left(-\frac{E_z}{c} \right) + \left(\frac{E_x}{c} \right) (B_y) + \left(\frac{E_y}{c} \right) (-B_x) + \left(\frac{E_z}{c} \right) (0) = \frac{1}{c} (E_x B_y - E_y B_x) \end{aligned}$$

$$\begin{aligned} S^{13} &\equiv F^{1\sigma} F^3_{\sigma} = -F^{10} F^{30} + F^{11} F^{31} + F^{12} F^{32} + F^{13} F^{33} \\ &= -\left(-\frac{E_x}{c} \right) \left(\frac{E_z}{c} \right) + (0) (B_y) + (B_z) (-B_x) + (-B_y) (0) = -\left(\frac{E_x E_z}{c^2} + B_x B_z \right) \end{aligned}$$

$$\begin{aligned} S^{23} &\equiv F^{2\sigma} F^3_{\sigma} = -F^{20} F^{30} + F^{21} F^{31} + F^{22} F^{32} + F^{23} F^{33} \\ &= -\left(-\frac{E_y}{c} \right) \left(\frac{E_z}{c} \right) + (-B_z) (B_y) + (0) (-B_x) + (B_x) (0) = -\left(\frac{E_y E_z}{c^2} + B_y B_z \right) \end{aligned}$$

$$\begin{aligned} S^{33} &\equiv F^{3\sigma} F^3_{\sigma} = -F^{30} F^{30} + F^{31} F^{31} + F^{32} F^{32} + F^{33} F^{33} \\ &= -\left(-\frac{E_z}{c} \right) \left(-\frac{E_z}{c} \right) + (B_y) (B_y) + (-B_x) (-B_x) + (0) (0) = -\frac{E_z^2}{c^2} + B_x^2 + B_y^2 \end{aligned}$$

Thus, collecting our results for the {intermediate} tensor $S^{\mu\nu} \equiv F^{\mu\sigma} F^{\nu}_{\sigma}$:

$$S^{\mu\nu} \equiv F^{\mu\sigma} F^{\nu}_{\sigma} = \begin{pmatrix} S^{00} & S^{01} & S^{02} & S^{03} \\ S^{10} & S^{11} & S^{12} & S^{13} \\ S^{20} & S^{21} & S^{22} & S^{23} \\ S^{30} & S^{31} & S^{32} & S^{33} \end{pmatrix}$$

$$S^{\mu\nu} \equiv F^{\mu\sigma} F^{\nu}_{\sigma} = \begin{pmatrix} \frac{E^2}{c^2} & \frac{1}{c} (E_y B_z - E_z B_y) & \frac{1}{c} (E_z B_x - E_x B_z) & \frac{1}{c} (E_x B_y - E_y B_x) \\ \frac{1}{c} (E_y B_z - E_z B_y) & -\frac{E_x^2}{c^2} + B_y^2 + B_z^2 & -\left(\frac{E_x E_y}{c^2} + B_x B_y \right) & -\left(\frac{E_x E_z}{c^2} + B_x B_z \right) \\ \frac{1}{c} (E_z B_x - E_x B_z) & -\left(\frac{E_x E_y}{c^2} + B_x B_y \right) & -\frac{E_y^2}{c^2} + B_x^2 + B_z^2 & -\left(\frac{E_y E_z}{c^2} + B_y B_z \right) \\ \frac{1}{c} (E_x B_y - E_y B_x) & -\left(\frac{E_x E_z}{c^2} + B_x B_z \right) & -\left(\frac{E_y E_z}{c^2} + B_y B_z \right) & -\frac{E_z^2}{c^2} + B_x^2 + B_y^2 \end{pmatrix}$$

Note that $S^{\mu\nu}$ is a symmetric matrix, i.e. $S^{\mu\nu} = S^{\nu\mu}$ {which is good, because $T^{\mu\nu}$ is symmetric!}

$$S^{\mu\nu} \equiv F^{\mu\sigma} F^{\nu}_{\sigma} \quad \text{and:} \quad S^{\nu\mu} \equiv F^{\nu\sigma} F^{\mu}_{\sigma}$$

$\therefore \boxed{F^{\mu\sigma} F^\nu{}_\sigma = F^{\nu\sigma} F^\mu{}_\sigma}$ and since each $\boxed{F^{\mu\sigma} F^\nu{}_\sigma}$, or equivalently $\boxed{F^{\nu\sigma} F^\mu{}_\sigma}$ is the sum of 4 terms ($\sigma = 0:3$) then we may also write these as: $\boxed{F^{\mu\nu} F^\nu{}_\sigma = F^\nu{}_\sigma F^{\mu\sigma}}$ and: $\boxed{F^{\nu\sigma} F^\mu{}_\sigma = F^\mu{}_\sigma F^{\nu\sigma}}$.

$$\therefore \boxed{S^{\mu\nu} = S^{\nu\mu} = F^{\mu\sigma} F^\nu{}_\sigma = F^{\nu\sigma} F^\mu{}_\sigma = F^\nu{}_\sigma F^{\mu\sigma} = F^\mu{}_\sigma F^{\nu\sigma}}$$

Then:
$$\boxed{T^{\mu\nu} \equiv \epsilon_0 c^2 \left[\underbrace{(F^{\mu\sigma} F^\nu{}_\sigma)}_{\equiv S^{\mu\nu}} - \frac{1}{4} \delta^{\mu\nu} \underbrace{(F_{\lambda\sigma} F^{\lambda\sigma})}_{= -2 \left(\frac{E^2}{c^2} - B^2 \right)} \right]}$$
 where:
$$\delta^{\mu\nu} \equiv \begin{pmatrix} -1 & 0 & 0 & 0 \\ 0 & +1 & 0 & 0 \\ 0 & 0 & +1 & 0 \\ 0 & 0 & 0 & +1 \end{pmatrix}$$

$$S^{\mu\nu} \equiv F^{\mu\sigma} F^\nu{}_\sigma = \begin{pmatrix} \frac{E^2}{c^2} & \frac{1}{c}(E_y B_z - E_z B_y) & \frac{1}{c}(E_z B_x - E_x B_z) & \frac{1}{c}(E_x B_y - E_y B_x) \\ \frac{1}{c}(E_y B_z - E_z B_y) & -\frac{E_x^2}{c^2} + B_y^2 + B_z^2 & -\left(\frac{E_x E_y}{c^2} + B_x B_y\right) & -\left(\frac{E_x E_z}{c^2} + B_x B_z\right) \\ \frac{1}{c}(E_z B_x - E_x B_z) & -\left(\frac{E_x E_y}{c^2} + B_x B_y\right) & -\frac{E_y^2}{c^2} + B_x^2 + B_z^2 & -\left(\frac{E_y E_z}{c^2} + B_y B_z\right) \\ \frac{1}{c}(E_x B_y - E_y B_x) & -\left(\frac{E_x E_z}{c^2} + B_x B_z\right) & -\left(\frac{E_y E_z}{c^2} + B_y B_z\right) & -\frac{E_z^2}{c^2} + B_x^2 + B_y^2 \end{pmatrix}$$

Note that since $\delta^{\mu\nu}$ only contributes to the diagonal elements of $T^{\mu\nu}$, let us compute these:

$$\begin{aligned} T^{00} &= \epsilon_o c^2 \left[S^{00} - \frac{1}{4} 2 \left(\frac{E^2}{c^2} - B^2 \right) \right] = \epsilon_o c^2 \left[\frac{E^2}{c^2} - \frac{1}{2} \left(\frac{E^2}{c^2} - B^2 \right) \right] \\ &= \epsilon_o c^2 \left[\frac{1}{2} \frac{E^2}{c^2} + \frac{1}{2} B^2 \right] = \frac{1}{2} \epsilon_o E^2 + \frac{1}{2} \epsilon_o c^2 B^2 = \frac{1}{2} \epsilon_o E^2 + \frac{1}{2 \mu_o} B^2 = u_{EM} \end{aligned}$$

$$\begin{aligned} T^{11} &= \epsilon_o c^2 \left[S^{11} + \frac{1}{4} 2 \left(\frac{E^2}{c^2} - B^2 \right) \right] = \epsilon_o c^2 \left[-\frac{E_x^2}{c^2} + B_y^2 + B_z^2 + \frac{1}{2} \frac{E^2}{c^2} - \frac{1}{2} B^2 \right] \\ &= \epsilon_o c^2 \left[-\frac{E_x^2}{c^2} + \frac{1}{2} \left(\frac{E_x^2}{c^2} + \frac{E_y^2}{c^2} + \frac{E_z^2}{c^2} \right) + B_y^2 + B_z^2 - \frac{1}{2} (B_x^2 + B_y^2 + B_z^2) \right] \\ &= \epsilon_o c^2 \left[\frac{1}{2} \left(-\frac{E_x^2}{c^2} + \frac{E_y^2}{c^2} + \frac{E_z^2}{c^2} \right) + \frac{1}{2} (-B_x^2 + B_y^2 + B_z^2) \right] = \frac{\epsilon_o c^2}{2} \left[\left(-\frac{E_x^2}{c^2} + \frac{E_y^2}{c^2} + \frac{E_z^2}{c^2} \right) \right] \\ &= \frac{1}{2} \epsilon_o c^2 \left[\left(-\frac{E_x^2}{c^2} + \frac{E_y^2}{c^2} + \frac{E_z^2}{c^2} \right) + (-B_x^2 + B_y^2 + B_z^2) \right] \\ &= -\frac{1}{2} \epsilon_o c^2 \left[\left(\frac{E_x^2}{c^2} - \frac{E_y^2}{c^2} - \frac{E_z^2}{c^2} \right) + (B_x^2 - B_y^2 - B_z^2) \right] = -\epsilon_o c^2 \left[\left(\frac{E_x^2}{c^2} + B_x^2 \right) - \frac{1}{2} \left(\frac{E^2}{c^2} + B^2 \right) \right] \end{aligned}$$

From the above elements S^{11}, S^{22}, S^{33} and their cyclic permutation symmetries we see that:

$$T^{22} = -\frac{1}{2} \epsilon_o c^2 \left[\left(-\frac{E_x^2}{c^2} + \frac{E_y^2}{c^2} - \frac{E_z^2}{c^2} \right) + (-B_x^2 + B_y^2 - B_z^2) \right] = -\epsilon_o \left[\left(\frac{E_y^2}{c^2} + B_y^2 \right) - \frac{1}{2} \left(\frac{E^2}{c^2} + B^2 \right) \right]$$

and:

$$T^{33} = -\frac{1}{2} \epsilon_o c^2 \left[\left(-\frac{E_x^2}{c^2} - \frac{E_y^2}{c^2} + \frac{E_z^2}{c^2} \right) + (-B_x^2 - B_y^2 + B_z^2) \right] = -\epsilon_o \left[\left(\frac{E_z^2}{c^2} + B_z^2 \right) - \frac{1}{2} \left(\frac{E^2}{c^2} + B^2 \right) \right]$$

Then for all other remaining elements of the relativistic version of Maxwell's stress tensor,

$$T^{\mu\nu} \Big|_{\mu \neq \nu}, \text{ we see that since: } \left[\delta^{\mu\nu} \Big|_{\mu \neq \nu} = 0 \right] \text{ then: } \left[T^{\mu\nu} \Big|_{\mu \neq \nu} = \epsilon_o c^2 \left(F^{\mu\sigma} F_{\sigma}^{\nu} \right) \Big|_{\mu \neq \nu} = \epsilon_o c^2 S^{\mu\nu} \Big|_{\mu \neq \nu} \right]$$

Thus:

$$T^{\mu\nu} = \begin{pmatrix} \frac{1}{2} \epsilon_o c^2 \left(\frac{E^2}{c^2} + B^2 \right) = u_{EM} & \epsilon_o c (E_y B_z - E_z B_y) & \epsilon_o c (E_z B_x - E_x B_z) & \epsilon_o c (E_x B_y - E_y B_x) \\ \epsilon_o c (E_y B_z - E_z B_y) & -\epsilon_o c \left[\left(\frac{E_x^2}{c^2} + B_x^2 \right) - \frac{1}{2} \left(\frac{E^2}{c^2} + B^2 \right) \right] & -\epsilon_o c^2 \left[\left(\frac{E_x E_y}{c^2} \right) + B_x B_y \right] & -\epsilon_o c^2 \left[\left(\frac{E_x E_z}{c^2} \right) + B_x B_z \right] \\ \epsilon_o c (E_z B_x - E_x B_z) & -\epsilon_o c^2 \left[\left(\frac{E_x E_y}{c^2} \right) + B_x B_y \right] & -\epsilon_o c \left[\left(\frac{E_y^2}{c^2} + B_y^2 \right) - \frac{1}{2} \left(\frac{E^2}{c^2} + B^2 \right) \right] & -\epsilon_o c^2 \left[\left(\frac{E_y E_z}{c^2} \right) + B_y B_z \right] \\ \epsilon_o c (E_x B_y - E_y B_x) & -\epsilon_o c^2 \left[\left(\frac{E_x E_z}{c^2} \right) + B_x B_z \right] & -\epsilon_o c^2 \left[\left(\frac{E_y E_z}{c^2} \right) + B_y B_z \right] & -\epsilon_o c^2 \left[\left(\frac{E_z^2}{c^2} + B_z^2 \right) - \frac{1}{2} \left(\frac{E^2}{c^2} + B^2 \right) \right] \end{pmatrix}$$

Now Poynting's vector:

$$\begin{aligned} \vec{S} &= \frac{1}{\mu_o} (\vec{E} \times \vec{B}) = \epsilon_o c^2 (\vec{E} \times \vec{B}) = \epsilon_o c^2 \left[(\vec{E} \times \vec{B})_x \hat{x} + (\vec{E} \times \vec{B})_y \hat{y} + (\vec{E} \times \vec{B})_z \hat{z} \right] \\ &= \epsilon_o c^2 \left[(E_y B_z - E_z B_y) \hat{x} + (E_z B_x - E_x B_z) \hat{y} + (E_x B_y - E_y B_x) \hat{z} \right] \end{aligned}$$

$$\text{Thus: } \frac{1}{c} \vec{S} = \epsilon_o c \left[(E_y B_z - E_z B_y) \hat{x} + (E_z B_x - E_x B_z) \hat{y} + (E_x B_y - E_y B_x) \hat{z} \right]$$

But relativistic linear momentum density $\vec{\wp} = \frac{1}{c^2} \vec{S}$ or: $\vec{\wp} c = \frac{1}{c} \vec{S}$. Thus, we see that:

$$\begin{aligned} T^{00} &= u_{EM} & T^{01} &= \frac{1}{c} S_x = \wp_x c = T^{10} & T^{02} &= \frac{1}{c} S_y = \wp_y c = T^{20} & T^{03} &= \frac{1}{c} S_z = \wp_z c = T^{30} \\ T^{10} &= \wp_x c = \frac{1}{c} S_x = T^{01} \\ T^{20} &= \wp_y c = \frac{1}{c} S_y = T^{02} \\ T^{30} &= \wp_z c = \frac{1}{c} S_z = T^{03} \end{aligned}$$

Thus: $T^{\mu\nu} \equiv \epsilon_0 c^2 \left[\left(F^{\mu\sigma} F^\nu{}_\sigma \right) - \frac{1}{4} \delta^{\mu\nu} \left(F_{\lambda\sigma} F^{\lambda\sigma} \right) \right]$ gives:

$$T^{\mu\nu} = \begin{pmatrix} u_{EM} & \frac{1}{c} S_x & \frac{1}{c} S_y & \frac{1}{c} S_z \\ \rho_x c & -\epsilon_0 c \left[\left(\frac{E_x^2}{c^2} + B_x^2 \right) - \frac{1}{2} \left(\frac{E^2}{c^2} + B^2 \right) \right] & -\epsilon_0 c^2 \left[\left(\frac{E_x E_y}{c^2} \right) + B_x B_y \right] & -\epsilon_0 c^2 \left[\left(\frac{E_x E_z}{c^2} \right) + B_x B_z \right] \\ \rho_y c & -\epsilon_0 c^2 \left[\left(\frac{E_x E_y}{c^2} \right) + B_x B_y \right] & -\epsilon_0 c \left[\left(\frac{E_y^2}{c^2} + B_y^2 \right) - \frac{1}{2} \left(\frac{E^2}{c^2} + B^2 \right) \right] & -\epsilon_0 c^2 \left[\left(\frac{E_y E_z}{c^2} \right) + B_y B_z \right] \\ \rho_z c & -\epsilon_0 c^2 \left[\left(\frac{E_x E_z}{c^2} \right) + B_x B_z \right] & -\epsilon_0 c^2 \left[\left(\frac{E_y E_z}{c^2} \right) + B_y B_z \right] & -\epsilon_0 c^2 \left[\left(\frac{E_z^2}{c^2} + B_z^2 \right) - \frac{1}{2} \left(\frac{E^2}{c^2} + B^2 \right) \right] \end{pmatrix}$$

The classical electrodynamics 3-D force density is:

$$\vec{f} = \vec{\nabla} \cdot \vec{T} - \frac{1}{c^2} \frac{\partial \vec{S}}{\partial t} = -\frac{\partial \left(\frac{1}{c} \vec{S} \right)}{\partial (ct)} + \vec{\nabla} \cdot \vec{T}$$

SI units:
 N/m^3

where: $\vec{f} = f_x \hat{x} + f_y \hat{y} + f_z \hat{z}$

But: $T^{\mu\nu} \big|_{\mu,\nu=1:3} = -\vec{T}_{ij} \big|_{i,j=1:3}$ and: $-\frac{\partial \left(\frac{1}{c} \vec{S} \right)}{\partial (ct)} = -\frac{\partial \left(\frac{1}{c} S_x \hat{x} + \frac{1}{c} S_y \hat{y} + \frac{1}{c} S_z \hat{z} \right)}{\partial x^0} = -\frac{\partial (T^{01} \hat{x} + T^{02} \hat{y} + T^{03} \hat{z})}{\partial x^0}$

The relativistic electrodynamics force density 4-vector is: $f^\nu = (f^0, \vec{f})$ (SI units: N/m^3)

The zeroth/temporal/scalar component of the 4-vector f^ν is:

$$f^0 = -\frac{\partial (T^{00})}{\partial x^0} = -\frac{\partial (u_{EM})}{\partial (ct)}$$

Thus, the relativistic electrodynamics force density 4-vector is:

$$f^\nu = -\partial_\mu T^{\mu\nu} = -\frac{\partial T^{\mu\nu}}{\partial x^\mu} = -\left(\frac{\partial T^{0\nu}}{\partial x^0} + \frac{\partial T^{1\nu}}{\partial x^1} + \frac{\partial T^{2\nu}}{\partial x^2} + \frac{\partial T^{3\nu}}{\partial x^3} \right) \text{ where: } \partial_\mu \equiv \frac{\partial}{\partial x^\mu} \text{ is the covariant 4-D gradient operator.}$$

The total relativistic force 4-vector can likewise be obtained by noting that the 3-D spatial classical electrodynamics version of the 3-D total force vector is:

$$\vec{F} = \int_v \vec{f} d\tau = \int_v \left(-\frac{1}{c^2} \frac{\partial \vec{S}}{\partial t} + \vec{\nabla} \cdot \vec{T} \right) = \int_v \left(-\frac{\partial \left(\frac{1}{c} \vec{S} \right)}{\partial (ct)} + \vec{\nabla} \cdot \vec{T} \right) d\tau$$

Thus: $F^\nu = \int_{v_4} f^\nu d\tau_4 = -\int_{v_4} \partial_\mu T^{\mu\nu} d\tau_4 = -\int_{v_4} \left(\frac{\partial T^{\mu\nu}}{\partial x^\mu} \right) d\tau_4$ where: $F^\nu = (F^0, \vec{F})$ and:

The 4-D space-time volume v_4 has volume element $d\tau_4 = c dt dx dy dz$

$$\vec{F} = F_x \hat{x} + F_y \hat{y} + F_z \hat{z}$$

If one wishes to transform these results in one IRF(S) to another IRF(S') moving with relative velocity \vec{v} with respect to IRF(S), there are two equivalent methods to accomplish this task:

Method I:

First, Lorentz transform the \vec{E} and \vec{B} fields via:

$$\begin{pmatrix} \vec{E}' \\ \vec{B}' \end{pmatrix} = \underbrace{\begin{pmatrix} \gamma \left(1 - \left(\frac{\gamma}{\gamma+1} \right) \vec{\beta} \vec{\beta} \cdot \right) & \gamma \vec{\beta} x \\ -\gamma \vec{\beta} x & \gamma \left(1 - \left(\frac{\gamma}{\gamma+1} \right) \vec{\beta} \vec{\beta} \cdot \right) \end{pmatrix}}_{\text{n.b. operator matrix}} \begin{pmatrix} \vec{E} \\ \vec{B} \end{pmatrix} \quad \text{where:} \quad \begin{matrix} \gamma = \frac{1}{\sqrt{1-\beta^2}} \\ \vec{\beta} = \frac{\vec{v}}{c} \end{matrix}$$

See/read P436
Lecture Notes 19
for further details
of this method.

Then compute the new $F'^{\mu\nu}$, $S'^{\mu\nu} = F'^{\mu\sigma} F'^{\nu}_{\sigma}$ and $F'_{\lambda\sigma} F'^{\lambda\sigma}$ and thus compute the new $T'^{\mu\nu}$ in IRF(S'):

$$T'^{\mu\nu} = \epsilon_0 c^2 \left[\left(F'^{\mu\sigma} F'^{\nu}_{\sigma} \right) - \frac{1}{2} \delta^{\mu\nu} \left(F'_{\lambda\sigma} F'^{\lambda\sigma} \right) \right], \quad f'^{\nu} = -\frac{\partial T'^{\mu\nu}}{\partial x^{\mu}}, \quad F'^{\nu} = \int_{v_4} f'^{\nu} d\tau_4 = -\int_{v_4} \left(\frac{\partial T'^{\mu\nu}}{\partial x^{\mu}} \right) d\tau_4$$

This method has the advantage that all quantities, e.g. $\vec{E}', \vec{B}', \vec{S}', \vec{\phi}'$, $F'^{\mu\nu}$, $S'^{\mu\nu} = F'^{\mu\sigma} F'^{\nu}_{\sigma}$, $T'^{\mu\nu}$, f'^{ν} and F'^{ν} are explicitly known/calculated in IRF(S').

Method II:

Lorentz transform $T^{\mu\nu}$ directly, since the Lorentz transformation of $F^{\mu\nu}$ in IRF(S) to $F'^{\mu\nu}$ in IRF(S') moving with velocity \vec{v} relative to IRF(S) is given by: $F'^{\mu\nu} = \Lambda^{\mu}_{\lambda} \Lambda^{\nu}_{\sigma} F^{\lambda\sigma}$

Then: $T'^{\mu\nu} = \Lambda^{\mu}_{\lambda} \Lambda^{\nu}_{\sigma} T^{\lambda\sigma}$

Note that since: $T^{\mu\nu} = \epsilon_0 c^2 \left[\left(F^{\mu\sigma} F^{\nu}_{\sigma} \right) - \frac{1}{4} \delta^{\mu\nu} \left(F_{\lambda\sigma} F^{\lambda\sigma} \right) \right] = \epsilon_0 c^2 \left[S^{\mu\nu} - \frac{1}{4} \delta^{\mu\nu} \left(F_{\lambda\sigma} F^{\lambda\sigma} \right) \right]$

Then: $T'^{\mu\nu} = \Lambda^{\mu}_{\lambda} \Lambda^{\nu}_{\sigma} T^{\lambda\sigma} = \epsilon_0 c^2 \left[\Lambda^{\mu}_{\lambda} \Lambda^{\nu}_{\sigma} S^{\lambda\sigma} - \frac{1}{4} \Lambda^{\mu}_{\lambda} \Lambda^{\nu}_{\sigma} \delta^{\lambda\sigma} \left(F_{\lambda\sigma} F^{\lambda\sigma} \right) \right]$

Recall that: $\left(F_{\lambda\sigma} F^{\lambda\sigma} \right) = \left(F^{\lambda\sigma} F_{\lambda\sigma} \right) = -2 \left(\frac{E^2}{c^2} - B^2 \right) = \text{relativistic invariant}$ i.e. $F_{\lambda\sigma} F^{\lambda\sigma} = F'_{\lambda\sigma} F'^{\lambda\sigma} = \text{same value in any/all IRF'S!!!}$

Define: $S'^{\mu\nu} \equiv \Lambda^{\mu}_{\lambda} \Lambda^{\nu}_{\sigma} S^{\lambda\sigma}$ and $\delta'^{\mu\nu} \equiv \Lambda^{\mu}_{\lambda} \Lambda^{\nu}_{\sigma} \delta^{\lambda\sigma}$

Also note that ϵ_0 and c^2 , μ_0 are relativistically invariant scalar quantities (same in all IRF's)

Then: $T'^{\mu\nu} = \epsilon_0 c^2 \left[S'^{\mu\nu} - \frac{1}{4} \delta'^{\mu\nu} \left(F'_{\lambda\sigma} F'^{\lambda\sigma} \right) \right]$

Once $T'^{\mu\nu}$ is obtained, calculate $f'^{\nu} = -\frac{\partial T'^{\mu\nu}}{\partial x^{\mu}}$ and $F'^{\nu} = \int_{v_4} f'^{\nu} d\tau_4 = -\int_{v_4} \left(\frac{\partial T'^{\mu\nu}}{\partial x^{\mu}} \right) d\tau_4$